

On Weight-Prioritized Multitask Control of Humanoid Robots

Karim Bouyarmane ¹⁰, Member, IEEE, and Abderrahmane Kheddar ¹⁰, Senior Member, IEEE

Abstract—We propose a formal analysis with some theoretical properties of weight-prioritized multitask inversedynamics-like control of humanoid robots, being a case of redundant "manipulators" with a nonactuated free-floating base and multiple unilateral frictional contacts with the environment. The controller builds on a weighted-sum scalarization of a multiobjective optimization problem under equality and inequality constraints, which appears as a straightforward solution to account for state and control input viability constraint characteristic of humanoid robots that were usually absent from early existing pseudoinverse and nullspace projection-based prioritized multitask approaches. We argue that our formulation is indeed well founded and justified from a theoretical standpoint, and we propose an analysis of some stability properties of the approach. Lyapunov stability is demonstrated for the closed-loop dynamical system that we analytically derive in the unconstrained multiobjective optimization case. Stability in terms of solution existence, uniqueness, continuity, and robustness to perturbations is then formally demonstrated for the constrained quadratic program.

Index Terms—Lyapunov's indirect method, multiobjective optimization, multitask control, quadratic-program (QP) stability.

I. INTRODUCTION

PPLYING early control methods developed for (industrial) manipulators [1], [2] to humanoid robots, e.g., inverse dynamics control, operational or task function space control, etc., raises a number of challenging problems [3]–[6]. Typical such problems include simultaneous resolution of redundancy and underactuation or actuation through friction-cone-constrained unilateral contact forces. Although each of these problems has already been extensively studied in the

Manuscript received July 1, 2016; revised February 19, 2017, July 29, 2017, and August 16, 2017; accepted August 27, 2017. Date of publication September 13, 2017; date of current version May 23, 2018. This work was supported in parts by grants of the COMANOID EU H2020 project (www.comanoid.eu) and of the Japan Society for Promotion of Science Grant-in-Aid for Scientific Research, Kakenhi B No. 16H02886. Recommended by Associate Editor H. G. Tanner. (Corresponding author: Karim Bouyarmane.)

K. Bouyarmane is with the Larsen Team, Loria UMR 7503, CNRS, Inria, Université de Lorraine, F-54500 Vandœuvre-lès-Nancy, France (e-mail: karim.bouyarmane@gmail.com).

A. Kheddar is with the LIRMM Interactive Digital Humans Group, CNRS-University of Montpellier, 34095 Montpellier, France, and also with CNRS-AIST Joint Robotics Laboratory UMI3218/RL, Tsukuba 305-8568, Japan (e-mail: kheddar@gmail.com).

Color versions of one or more of the figures in this paper are available online at http://ieeexplore.ieee.org.

Digital Object Identifier 10.1109/TAC.2017.2752085

context of industrial manipulators or various general cases (e.g., handling redundancy in [7] and [8], underactuation in [9] and [10], contacts constraints in [11]–[14], bounds on control inputs in [15], and references therein), the specificity of a humanoid robot is that it features and interleaves them all at once and, thus, renders the solutions that were proposed for each of these problems taken in a separate setting largely inapplicable in a unified control framework.

We tackle these combined structural problems in a simple formulation, in which we make the nonequivocal distinction between the two notions of constraints and tasks, a distinction that we believe should be made by/in any humanoid control law design at large. Constraints are inherent to the well-posedness of the problem, as failing to satisfy them results in a physically or mathematically ill-posed problem. These are the physics laws (Newton-Euler equations or Lagrange equations, Coulomb laws) and the safety and structural limits (torque saturation, joint angle and velocity limits, and collision and obstacle avoidance). Tasks, on the other hand, allow for more tolerance in their fulfillment and necessitate a certain degree of "compliance" in their execution. Failing to realize them does not result in a mathematical or physical law violation. Since tasks come one way or another from planning (offline or real time), then it should be the role of the *planner*, not the controller, to ensure that the tasks are consistent and realizable [16].

Another important aspect in which humanoids differ essentially from industrial manipulators is their novel context of applications. An industrial manipulator is confined to a structured, known, and uncertainty-free environment. It is thus conceivable that, in that setting, tasks are seen as constraints that should be realized perfectly, more so if the manipulator had been specifically designed for the task at hand. Humanoids, even when targeted to manufacturing, are neither customized to achieve a particular task nor do they evolve in a structured environment that was exclusively designed for their operations. As such, tasks shall have the flexibility to be set as constraints or as objectives to be realized at best given their actual structural constraints and the uncertain state of their environment.

In this paper, we have taken a step back from what we already extensively achieve in experimental humanoid robotics. First, we adapt in an original way, different from the recursive null-space projection approach, the inverse dynamics control principles to general multitask systems and to the "humanoid type of manipulator" in particular accounting for its redundant, underactuated, and constrained nature (e.g., walking stability). Second, we assess the foundations from a control theoretical perspective of such control schemes. This constitues our novel contribution with respect to the existing work.

¹www.comanoid.eu

II. MAIN RESULTS AND STRUCTURE OF THIS PAPER

In Section III-A, we cast the problem of multitask control as a multiobjective optimization problem. Proposition 1 explores the one-task control case and its exact realization if unconstrained. When there are multiple tasks competing with each other, their exact realization cannot be guaranteed anymore, but under the conditions in Section III-B, we can approach the realization of a desired task at a given precision. Proposition 2 explores the meaning and consequences of not realizing exactly a desired task but approaching it at the given precision. We show that this results in a uniformly ultimately bounded (UUB) task error that converges to zero in some circumstances.

In Section III-B, we recall for the unfamiliar reader some main results from the multiobjective optimization literature that drive our reasoning (see Theorems 1–7). We then derive results under which Proposition 2 is applicable, namely Corollary 2: if a task is realizable exactly (when considered alone), then when put in competition with the other tasks, there exists a set of weights that makes it realizable at any desired precision.

In Section IV, we study the unconstrained dynamical system's ordinary differential equation (ODE) that results from the weighted-sum scalarization of the multiobjective optimization, as formulated in Section III. The main result is Proposition 4, which characterizes the equilibrium point and gives necessary and sufficient conditions for its exponential stability. The methodology followed in the proof of Proposition 4 is first introduced for the simpler one-task setting in Proposition 3.

In Section V, we consider the multitask control problem of a humanoid robot. Proposition 5 allows us to position the problem within the context of the framework developed in Section III-B (thanks to results borrowed from Theorems 9 and 10). In this section, we consider the full constrained humanoid problem and formulate it as a linearly constrained quadratic program (QP). The results in Propositions 6–9 and Corollary 5 then give us conditions for the well-posedness, robustness to perturbations, and continuity of the solution of that QP.

Note: We label "Theorem" any result that we borrow from the literature and "Proposition," "Corollary," and "Lemma" results that we propose as contribution. We also borrow all the "Definitions" from the literature, as we do not redefine any of the literature terminology.

III. MULTITASK CONTROL AS A MULTIOBJECTIVE OPTIMIZATION PROBLEM

A. General Concepts

Let us recall some concepts of multiobjective optimization (also known as multicriteria optimization, multiple-criteria decision making, and vector optimization [17], [18]) and demonstrate some useful properties in our context of multitask control. Multiobjective optimization studies the problem

$$\min_{x \in \mathcal{X}} f(x) = (f_1(x), \dots, f_p(x)) \tag{1}$$

where the min operator is put between quotation marks to emphasize that it is dependent on some specific optimality notion for vector values to be defined. The $f_{1,2,\cdots,p}$ functions are scalar functions and \mathcal{X} is the feasible space (e.g., as defined by a set of constraints on x). A solution $x^* \in \mathcal{X}$ of (1) is called an *efficient* (or *Pareto-optimal*) solution if there is no $x \in \mathcal{X}$ such that

 $f(x) \leq f(x^*)$. The notation $y^1 \leq y^2$ denotes the *component-wise* order in \mathbb{R}^p .

Definition 1 (Componentwise order [17, Definition 2.1, p. 24]): Let y^1 and y^2 be two vectors of \mathbb{R}^p . y^2 is said to be dominated² by y^1 , and we denote $y^1 \leq y^2$, if $\forall k \in \{1, \dots, p\}$ $y_k^1 \leq y_k^2$ and $y^1 \neq y^2$, i.e., at least one inequality holds strictly $\exists i \in \{1, \dots, p\}$ $y_i^1 < y_i^2$.

This notion of componentwise order is to be clearly distinguished from the *weak* and *strict* componentwise orders that we also use in the developments to follow.

Definition 2 (Weak componentwise order [17, Definition 2.24, p. 38]): y^2 is said to be weakly dominated by y^1 , and we denote $y^1 \leq y^2$, if $\forall k \in \{1, \dots, p\}$ $y_k^1 \leq y_k^2$.

Definition 3 (Strict componentwise order [17, Definition 2.24, p. 38]): y^2 is said to be strictly dominated by y^1 , and we denote $y^1 < y^2$, if $\forall k \in \{1, \dots, p\}$ $y_k^1 < y_k^2$. Let $\mathcal{Y} = f(\mathcal{X}) \subset \mathbb{R}^p$ denote the image of the feasible set.

Let $\mathcal{Y} = f(\mathcal{X}) \subset \mathbb{R}^p$ denote the image of the feasible set. If x^* is an efficient solution of (1), then its image $y^* = f(x^*)$ is called a *nondominated* point of \mathcal{Y} . The set of all efficient solutions of (1) is denoted \mathcal{X}_E , and the set of all nondominated points of \mathcal{Y} is denoted \mathcal{Y}_N (sometimes referred to as the *Pareto-optimal front*). We denote

$$y^{I} = \left(\min_{x \in \mathcal{X}} f_{1}(x), \dots, \min_{x \in \mathcal{X}} f_{p}(x)\right)$$
 (2)

the so-called *ideal point*. In general, the ideal point is not realizable, i.e., $y^I \notin \mathcal{Y}$, in that case any point in \mathcal{Y}_N can be seen as a nonimprovable compromise solution of (1) (note that if, however, $y^I \in \mathcal{Y}$, then \mathcal{Y}_N reduces to the singleton $\{y^I\}$, i.e., $y^I \in \mathcal{Y} \Leftrightarrow \mathcal{Y}_N = \{y^I\}$).

In a context of multitask control with p tasks, each task τ_k $(k \in \{1,\ldots,p\})$ is defined through a forward kinematics function $g_k: \mathbb{R}^n \to \mathbb{R}^{n_k}$, mapping the n-dimensional generalized coordinates of the system q to the n_k -dimensional value of the task $\tau_k = g_k(q)$ $(n \geq n_k)$. A task is associated with a planned reference trajectory $t \mapsto \tau_k^r(t)$ and an objective attractor behavior to realize exponential tracking of the reference trajectory. In the case of a humanoid robot system as will be considered in Section V, the tasks τ_k of interest are of vector relative degree 2. This is due to the fact that they explicitly depend only on the configuration variable q (and not on the velocity \dot{q}), and that the dynamics model of the robot is of second order (see Section V). Hence, we consider throughout this paper tasks of vector relative degree 2. Denoting the task error $e_k = \tau_k - \tau_k^r$, the attractor behavior takes the form

$$\ddot{e}_k + D_k \dot{e}_k + P_k e_k = 0 \tag{3}$$

where the matrices (P_k, D_k) are so that $(\underline{0}_{P_k} I_{n_k} D_k)$ is *stable* (i.e., has all its eigenvalues with negative real parts).

 $^{^2\}mathrm{Note}$ the nonintuitive use of the "dominated by" terminology. y^2 is dominated by y^1 in the sense that y^2 is less optimal than y^1 , thus dominated by y^1 in the optimality characteristic.

For convenience of notation, the behavior (3) can also be written in the form

$$\ddot{\tau}_k - \ddot{\tau}_k^d = 0 \tag{4}$$

with the desired task acceleration $\ddot{\tau}_k^d = \ddot{\tau}_k^r - D_k \dot{e}_k - P_k e_k$. If the constraints of the robot make it impossible to achieve perfect realization of $\ddot{\tau}_k^d$, then one might want to realize this behavior "at best" in the following sense:

$$\min_{x \in \mathcal{X}} \|\ddot{\tau}_k - \ddot{\tau}_k^d\|^2 \tag{5}$$

where x denotes a control decision variable and $x \in \mathcal{X}$ its constraints. As we will see later (see Section V), the particular choice of the square norm $\|\cdot\|^2$ allows us to formulate the problem as a linearly constrained QP and use algorithms that are dedicated to this class of optimization problems. Let $J_k = \partial g_k/\partial q \in \mathbb{R}^{n_k \times n}$ denote the Jacobian matrix of the task $\tau_k = g_k(q)$. Here and henceforth, we suppose that g_k is continuously differentiable so that J_k exists and is continuous (which is always the case for a large class of robotic systems in practice). In the simplest case, where $x = \ddot{q}$ and $\mathcal{X} = \mathbb{R}^n$, we can easily show the following.

Proposition 1: If J_k is full row rank, then (5) \Leftrightarrow (4). Proof: The first-order optimality condition for (5) is

$$\frac{\partial \|\ddot{\tau}_k - \ddot{\tau}_k^d\|^2}{\partial \ddot{a}} = 0 \tag{6}$$

$$\Leftrightarrow \frac{\partial \left(\ddot{\tau}_{k} - \ddot{\tau}_{k}^{d}\right)^{T}}{\partial \ddot{q}} (\ddot{\tau}_{k} - \ddot{\tau}_{k}^{d}) + (\ddot{\tau}_{k} - \ddot{\tau}_{k}^{d})^{T} \frac{\partial \left(\ddot{\tau}_{k} - \ddot{\tau}_{k}^{d}\right)}{\partial \ddot{q}} = 0$$

$$\Leftrightarrow 2\frac{\partial (\ddot{\tau}_k - \ddot{\tau}_k^d)}{\partial \ddot{q}}^T (\ddot{\tau}_k - \ddot{\tau}_k^d) = 0.$$
 (8)

Since $\dot{\tau}_k = J_k \dot{q}$ and $\ddot{\tau}_k = J_k \ddot{q} + \dot{J}_k \dot{q}$, we have $\partial \ddot{\tau}_k / \partial \ddot{q} = J_k$ (tasks of vector relative degree two). On the other hand, $\partial \ddot{\tau}_k^d / \partial \ddot{q} = 0$. Hence

(8)
$$\Leftrightarrow$$
 $2J_k^T(\ddot{\tau}_k - \ddot{\tau}_k^d) = 0.$ (9)

By the rank-nullity theorem, $\dim \ker J_k^T = n_k - \operatorname{rank} J_k^T = n_k - \operatorname{rank} J_k$; since $\operatorname{rank} J_k = n_k$, then $\dim \ker J_k^T = 0$, which means $\ker J_k^T = \{0\}$; the desired equivalence thus follows from (9).

In the more general case, we can state the following.

Definition 4 (see [20], [21], [22, Definition 4.6, p. 169]): The solutions of a system $\dot{\chi} = \varphi(\chi,t)$ are said to be UUB if there exists b>0 and c>0 such that, for every 0< a< c, there exists T(a,b)>0 such that

$$\|\chi(0)\| < a \implies \forall t \ge T(a, b), \|\chi(t)\| < b.$$
 (10)

b is called an ultimate bound of the solutions. If a can be arbitrarily large, i.e., if there exists b>0 such that for every a>0 there exists T(a,b)>0 such that (10) holds, then the solutions are said to be globally UUB with ultimate bound b.

Let $\mu(A_k)$ denote the logarithmic norm of A_k associated with the vector norm $\|.\|$.

Definition 5 (see [23]): The logarithmic norm associated with the vector norm $\|.\|$ in \mathbb{R}^{2n_k} and its subordinate matrix

norm $\|.\|$ in $\mathbb{R}^{2n_k \times 2n_k}$ is defined as

$$\mu(A_k) = \lim_{h \to 0^+} \frac{\|I + hA_k\| - 1}{h}.$$
 (11)

It can be shown [24] that $\mu(A_k) = \lambda_{\max} \left[\frac{1}{2} (A_k + A_k^T) \right]$, the maximum eigenvalue of $\frac{1}{2} (A_k + A_k^T)$.

Proposition 2: If $A_k + A_k^T$ is negative definite, then, for any $\epsilon > 0$, the differential inequality

$$\|\ddot{\tau}_k - \ddot{\tau}_k^d\|^2 < \epsilon \tag{12}$$

results in $\eta_k(t)$ globally UUB. Moreover, for any $t \mapsto \varepsilon(t) > 0$ such that $\varepsilon(t) = O\left(e^{2\mu(A_k)t}\right)$, the differential inequality

$$\|\ddot{\tau}_k - \ddot{\tau}_k^d\|^2 < \varepsilon(t) \tag{13}$$

implies, for every initial condition $\eta_k(0)$,

$$\eta_k(t) \xrightarrow[t \to +\infty]{} 0.$$
 (14)

Proof: The inequality (12) can be rewritten as

$$\|\dot{\eta_k} - A_k \eta_k\| = \left\| \begin{pmatrix} 0 \\ \ddot{\tau}_k - \ddot{\tau}_k^d \end{pmatrix} \right\| = \|\ddot{\tau}_k - \ddot{\tau}_k^d\| < \sqrt{\epsilon} \quad (15)$$

which is equivalent to

$$\dot{\eta}_k = A_k \eta_k + \zeta(t) \tag{16}$$

with $\|\zeta(t)\| < \sqrt{\epsilon}$. From the properties of the logarithmic norm, it can be shown [23] that (16) implies

$$\|\eta_k(t)\| \le e^{t\mu(A_k)} \|\eta_k(0)\| + \int_0^t e^{(t-\theta)\mu(A_k)} \|\zeta(\theta)\| d\theta \quad (17)$$

$$\leq e^{t\mu(A_k)} \|\eta_k(0)\| + \int_0^t e^{(t-\theta)\mu(A_k)} \sqrt{\epsilon} d\theta$$
 (18)

$$= \left(\|\eta_k(0)\| + \frac{\sqrt{\epsilon}}{\mu(A_k)} \right) e^{t\mu(A_k)} - \frac{\sqrt{\epsilon}}{\mu(A_k)}. \tag{19}$$

Let $\delta>0$. We show that $\eta_k(t)$ is globally UUB with ultimate bound $-\frac{\sqrt{\epsilon}}{\mu(A_k)}+\delta$. So let a>0. From (19), $\|\eta_k(0)\|< a$ implies that

$$\|\eta_k(t)\| < \left(a + \frac{\sqrt{\epsilon}}{\mu(A_k)}\right)e^{t\mu(A_k)} - \frac{\sqrt{\epsilon}}{\mu(A_k)}.$$
 (20)

We also have $\mu(A_k) = \lambda_{\max}\left[\frac{1}{2}(A_k + A_k^T)\right]$. Since $A_k + A_k^T$ is negative definite, $\mu(A_k) < 0$, and hence, the right-hand side of (20) goes to $-\frac{\sqrt{\epsilon}}{\mu(A_k)}$ as t goes to $+\infty$. Therefore, there exists $T(a,\delta)$ such that $\forall t \geq T(a,\delta): \|\eta_k(t)\| < -\frac{\sqrt{\epsilon}}{\mu(A_k)} + \delta$, and we can conclude that $\eta_k(t)$ is globally UUB with ultimate bound $-\frac{\sqrt{\epsilon}}{\mu(A_k)} + \delta$.

In the case of (13) with $\varepsilon(t) = O\left(e^{2\mu(A_k)t}\right)$, there exists M > 0 such that $\varepsilon(t) < Me^{2\mu(A_k)t}$, so

$$\int_0^t e^{(t-\theta)\mu(A_k)} \sqrt{\varepsilon(\theta)} d\theta \le \int_0^t e^{(t-\theta)\mu(A_k)} M e^{\theta\mu(A_k)} d\theta \tag{21}$$

$$= Mte^{t\mu(A_k)}. (22)$$

Hence, (17) implies

$$\|\eta_k(t)\| \le (\|\eta_k(0)\| + Mt)e^{t\mu(A_k)}.$$
 (23)

Since $\mu(A_k) < 0$, the right-hand side of (23) goes to 0 as t goes to $+\infty$, and therefore, $\lim_{t\to +\infty} \eta_k(t) = 0$.

Following this train of thought, it appears now that the multitask problem can indeed be written as a multiobjective optimization problem as introduced earlier in this section

$$\min_{x \in \mathcal{X}} f(x) = (\|\ddot{\tau}_1 - \ddot{\tau}_1^d\|^2, \dots, \|\ddot{\tau}_p - \ddot{\tau}_p^d\|^2).$$
(24)

We, thus, provide in the following a complete characterization of all the efficient solutions of this problem.

B. Characterization of the Efficient Solutions

It can be shown that, to a certain extent that is precisely defined hereafter, all the efficient solutions of the multiobjective optimization problem (1) can be obtained by solving single-objective problems of the form

$$\min_{x \in \mathcal{X}} \sum_{k=1}^{p} w_k f_k(x). \tag{25}$$

The problem (25) is called a weighted-sum *scalarization* of the problem (1). Different results on the completeness of the characterization of the solutions of (1) can be obtained depending on whether we consider the nonidentically null scalar weights w_k of (25) as only nonnegative or as (strictly) positive (i.e., whether $0 \le w$ or 0 < w using the componentwise order notations of Section III-A). Let us denote the set of optimal points in $\mathcal Y$ that are spanned by the problems (25) in these two cases, respectively, as

$$S_0(\mathcal{Y}) = \left\{ y^* \in \mathcal{Y} \mid \sum_{k=1}^p w_k y_k^* = \min_{y \in \mathcal{Y}} \sum_{k=1}^p w_k y_k, \ 0 \le w \right\}$$
(26)

$$S(\mathcal{Y}) = \left\{ y^* \in \mathcal{Y} \mid \sum_{k=1}^p w_k y_k^* = \min_{y \in \mathcal{Y}} \sum_{k=1}^p w_k y_k, \ 0 < w \right\}.$$
(27)

We need a few more definitions to complete those already introduced in Section III-A. A solution $x^* \in \mathcal{X}$ is said to be a weakly efficient solution of (1) if $f(x^*)$ is weakly nondominated in \mathcal{Y} , that is, if there is no $x \in \mathcal{X}$ such that $f(x) < f(x^*)$. The set of all weakly nondominated points in \mathcal{Y} is then denoted \mathcal{Y}_{wN} .

Theorem 1 (see [17, Th. 3.4, p. 69]): $S_0(\mathcal{Y}) \subset \mathcal{Y}_{wN}$.

For the converse inclusion, we need the following definition. *Definition 6 (see [17, Definition 3.1, p. 67] and [25,*

Definition 3.1, p. 329]): A set \mathcal{Y} is said to be \mathbb{R}^p_{\geq} -convex if $\mathcal{Y} + \mathbb{R}^p_{\geq}$ is convex. $\mathbb{R}^p_{\geq} = \{y \in \mathbb{R}^p \mid 0 \leq y\}$ is the nonnegative orthant.

Theorem 2 (see [17, Th. 3.5, p. 69]): If \mathcal{Y} is \mathbb{R}^p_{\geq} -convex, then $\mathcal{S}_0(\mathcal{Y}) = \mathcal{Y}_{wN}$.

Thus, we can see that under the conditions of Theorem 2, all weakly nondominated solutions of a multiobjective optimization problem can be obtained by weighted-sum scalarizations with nonnegative weights. In our coming formulation of multitask control, we need the weights to be positive for the sake of stability. Thus, we need stronger results, characterizing $\mathcal{S}(\mathcal{Y})$ rather than $\mathcal{S}_0(\mathcal{Y})$.

Theorem 3 (see [17, Th. 3.6, p. 70]): $S(\mathcal{Y}) \subset \mathcal{Y}_N$.

Unfortunately, the inclusion in Theorem 3 is too large, and the converse inclusion does not hold in general. In fact, it can be shown that the positive weights will only yield a set of the so-called *properly efficient* solutions.

Definition 7 (see [26, Definition, p. 618]): A solution $x^* \in \mathcal{X}$ is called properly efficient if it is efficient and $\exists M > 0$ s.t. $\forall x \in \mathcal{X}, \ \forall i \in \{1, \dots, p\} : f_i(x) < f_i(x^*) \Rightarrow \exists j \in \{1, \dots, p\} \setminus \{i\} \ s.t. \ f_j(x^*) < f_j(x) \ and$

$$\frac{f_i(x^*) - f_i(x)}{f_j(x) - f_j(x^*)} \le M.$$

In that case, the point $f(x^*)$ is said to be properly nondominated in \mathcal{Y} , and the set of all properly nondominated points of \mathcal{Y} is denoted \mathcal{Y}_{pN} .

Using Definition 7, a tighter inclusion than that of Theorem 3 can be obtained.

Theorem 4 (see [26, Th. 1]): $S(\mathcal{Y}) \subset \mathcal{Y}_{pN}$.

The converse inclusion of Theorem 4 holds.

Theorem 5 (see [17, Th. 3.13, p. 74]): If \mathcal{Y} is \mathbb{R}^p_{\geq} -convex, then $\mathcal{S}(\mathcal{Y}) = \mathcal{Y}_{pN}$.

Theorem 5 shows that only the properly efficient solutions of (1) can be attained with positive weights, and that this is the best we can achieve *exactly*. However, the following theorem, due to Hartley [27], allows us to *approximate* any efficient solution with positive-weight scalarization, which will prove useful in our application.

Definition 8 (see [18, Definition 3.2.4, p. 52]): A set \mathcal{Y} is said to be \mathbb{R}^p_{\geq} -closed if $\mathcal{Y} + \mathbb{R}^p_{\geq}$ is closed.

Theorem 6 (see [27, Th. 5.5]): If \mathcal{Y} is nonempty, \mathbb{R}^p_{\geq} -convex and \mathbb{R}^p_{\geq} -closed, then $\mathcal{Y}_N \subset \mathrm{cl}(\mathcal{S}(\mathcal{Y}))$.

Theorem $6\overline{i}$ s a powerful tool that allows us to perform our desired approximation. Before applying it, we will need the following lemma.

Lemma 1: There is always at least one efficient solution of problem (1) that exactly realizes a given component of the ideal point y^I (2), i.e., $\forall k \in \{1, ..., p\} \exists y \in \mathcal{Y}_N \text{ s.t. } y_k = y_k^I$.

problem (f) that exactly relatives a given component of the ractal point y^I (2), i.e., $\forall k \in \{1,\ldots,p\}$ $\exists y \in \mathcal{Y}_N$ s.t. $y_k = y_k^I$. Proof: Let k be a given index in $\{1,\ldots,p\}$. Let \mathcal{X}' denote the set $\mathcal{X}' = \{x \in \mathcal{X} \mid f_k(x) = y_k^I\}$, let $f': \mathcal{X}' \to \mathbb{R}^{p-1}$ such that $f'(x) = (f_1(x),\ldots,f_{k-1}(x),f_{k+1}(x),\ldots,f_p(x))$, and let y' be any nondominated point of $\mathcal{Y}' = f'(\mathcal{X}')$. Then, it is clear that y such that $y_k = y_k^I$ and $y_i = y_i'$ for $i \neq k$ satisfies the desired result.

Now, we state the following corollary, supposing in the remainder of this section that the conditions of Theorem 6 are satisfied.

Corollary 1: For any $\epsilon > 0$ and any index k, there exists a set of positive weights 0 < w such that $f_k(x^*) - y_k^I < \epsilon$, where x^* denotes a solution of problem (25).

Proof: From Lemma 1, there exists $y \in \mathcal{Y}_N$ such that $y_k = y_k^I$. From Theorem 6, we then have $y \in \operatorname{cl}(\mathcal{S}(\mathcal{Y}))$. Since \mathcal{Y} is finite dimensional, all norms are topologically equivalent, and thus, we can consider the ℓ^∞ -norm $\|.\|_\infty$ for the closure definition $\operatorname{cl}(.)$. Therefore, there exists a sequence of elements $(y^l)_{l\in\mathbb{N}}\in\mathcal{S}(\mathcal{Y})^\mathbb{N}$ such that $\|y^l-y\|_\infty \xrightarrow[l\to+\infty]{} 0$, and as such,

there exists $l_0 \in \mathbb{N}$ such that $\|y^{l_0} - y\|_{\infty} < \epsilon$. Finally, we have $y_k^{l_0} - y_k^I = y_k^{l_0} - y_k \le \|y^{l_0} - y\|_{\infty} < \epsilon$, which shows the desired result.

Applying Corollary 1 to problem (24) gives us the following.

Corollary 2: If a given task τ_k is realizable exactly, i.e., $\exists x \in \mathcal{X} \text{ s.t. } \ddot{\tau}_k = \ddot{\tau}_k^d$, then it can be reached with weighted-sum scalarization of (24) with positive weights at any given precision, i.e., for any $\epsilon > 0$, there exists 0 < w such that

$$\|\ddot{\tau}_k(x^*) - \ddot{\tau}_k^d\|^2 < \epsilon \tag{28}$$

where x^* is the solution of the w-weighted-sum scalarization of (24):

$$\min_{x \in \mathcal{X}} \sum_{l=1}^{p} w_l \| \ddot{\tau}_l(x) - \ddot{\tau}_l^d \|^2.$$
 (29)

Proof: Immediate from Corollary 1.

In redundant manipulator control, one popular optimality notion is what is usually referred to as the *strict priority* ordering of the tasks (or sometimes *strict hierarchy*), which is *de facto* imposed by the nature of the method itself, i.e., the recursive pseudoinversion of the task "constraint" and the projection in the null space of higher priority constrains [28]. In the context of multiobjective optimization, a similar notion is labeled under the term *lexicographic optimization*

$$\operatorname{lexmin}_{x \in \mathcal{X}} \left(f_1(x), \dots, f_p(x) \right) \tag{30}$$

which consists in finding a point $y^L \in \mathcal{Y}$ called the *lexicographic optimum* such that $\forall y \in \mathcal{Y} \ y^L \leq_{\text{lex}} y$ where \leq_{lex} denotes the *lexicographic order* (a total order) in \mathbb{R}^p .

Theorem 7 (see [17, Lemma 5.2, p. 129]): The lexicographic optimum is one particular efficient solution of (1), i.e., $y^L \in \mathcal{Y}_N$.

Applying again Theorem 6, we obtain the following.

Corollary 3: The lexicographic (strict priority) optimum can be approached at any given precision by positive weighted-sum scalarization, i.e., for any $\epsilon > 0$, there exists a set of positive weights 0 < w such that $||f(x^*) - y^L|| < \epsilon$, where x^* is the solution of (29).

Proof: Similar to the proof of Corollary 1 from Theorem 7. \blacksquare

At this stage, we have characterized the efficient solutions of (24) and justified the use of (29) for solving it. Propositions 1 and 2 give us some stability results in the state space of the tasks $(\tau_k, \dot{\tau}_k)$; we study in the following the behavior of the system in the state space of the generalized coordinates of the robot (q, \dot{q}) .

IV. STABILITY IN THE STATE SPACE OF THE GENERALIZED COORDINATES

In this section, we restrict ourselves to the case in which $x=\ddot{q}$ and $\mathcal{X}=\mathbb{R}^p$. This would provide us with some insight on the general case that is more complex to study analytically and is out of the scope of this paper. We also consider task function regulation problems, in which $t\mapsto \tau_k^r(t)$ are constant in time, and for ease of notation, we denote their constant regulation values τ_k^r .

Our aim here is to study the behavior of the system of ODEs defined by

$$\ddot{q} = \arg\min \sum_{k=1}^{p} w_k \| \ddot{\tau}_k - \ddot{\tau}_k^d \|^2$$
 (31)

in the state space of (q, \dot{q}) , where the weights are positive 0 < w following our analysis in Section III-B. As for related work concerning this section, see, for example, [29] and [30] that

study the stability of the strict priority inverse kinematics control approach, [7] and [28] for the stability of strict priority inverse dynamics, and [31] and [32] for the stability of the weighted approach of a multitask controller based on control Lyapunov functions.

We will base our argumentation below on Lyapunov's indirect method. In the Appendix, we introduce some general matrix differentiation concepts that we extensively use in the course of its application. This also allows us to introduce along the way the concept of the second derivative of the forward kinematics mapping (the "Jacobian of the Jacobian").

We start with a single-task case to illustrate our method in a simple setting; we then generalize the approach to multiple tasks. Note that some of the notations used throughout the rest of this paper are introduced inside the proofs of this section.

Proposition 3: Suppose $n_k = n$. The system

$$\ddot{q} = \arg\min \|\ddot{\tau}_k - \ddot{\tau}_k^d\|^2 \tag{32}$$

has an equilibrium if and only if there exists q^0 such that $g_k(q^0) = \tau_k^r$ and, in that case, if $J_k(q^0)$ is nonsingular, then the equilibrium is exponentially stable in the state space of (q,\dot{q}) . More generally, the system

$$\ddot{q} = \arg\min \|\dot{\eta}_k - A_k \eta_k\|^2 \tag{33}$$

where A_k is stable, has an equilibrium if and only if there exists q^0 such that $g_k(q^0) = \tau_k^r$ and, in that case, if $J_k(q^0)$ is nonsingular, then the equilibrium is exponentially stable in the state space of (q, \dot{q}) .

Proof: Let us denote by $\xi = (q, \dot{q})$ the state of the system (33). The variable ξ is related to η_k through the nonlinear "forward kinematics" mapping

$$\gamma_k : \xi \mapsto \eta_k = \gamma_k(\xi) = \begin{pmatrix} g_k(q) - \tau_k^r \\ J_k(q)\dot{q} \end{pmatrix}.$$
 (34)

Let $\mathcal{J}_k(\xi)$ denote the Jacobian matrix of that mapping at ξ . From (34), it appears that $\mathcal{J}_k(\xi)$ is related to $J_k(q)$ through the following relation:

$$\mathcal{J}_k(\xi) = \begin{pmatrix} J_k(q) & 0\\ \frac{\partial \left[J(q)\dot{q}\right]}{\partial q} & J_k(q) \end{pmatrix}. \tag{35}$$

From Proposition 1, the system (33) is equivalent to

$$\dot{\eta}_k = A_k \eta_k \tag{36}$$

which has an equilibrium if and only if there exists q^0 such that $\eta_k=0$, i.e., such that $g_k(q^0)=\tau_k^r$. In terms of ξ , (36) translates into the nonlinear *descriptor* system

$$\mathcal{J}_k(\xi)\dot{\xi} = A_k \gamma_k(\xi). \tag{37}$$

Let $\xi^0=(q^0,0)$. Since $n=n_k$ and $J_k(q^0)$ is nonsingular, we can see from (35) that $\mathcal{J}_k(\xi^0)$ is a square $2n\times 2n$ lower block triangular matrix with rank $\mathcal{J}_k(\xi^0)=\mathrm{rank}\,J_k(q^0)+\mathrm{rank}\,J_k(q^0)=2n$; therefore, $\mathcal{J}_k(\xi^0)$ is also nonsingular. Assuming that the forward kinematics mapping is continuously differentiable, then the mapping $\mathfrak{J}:\xi\mapsto \mathcal{J}_k(\xi)$ is continuous, and as such, the inverse image of any open set of $\mathbb{R}^{2n\times 2n}$ under \mathfrak{J} is open. Since the $GL_{2n}(\mathbb{R})$ group is an open subset of $\mathbb{R}^{2n\times 2n}$, $\mathfrak{J}^{-1}\left(GL_{2n}(\mathbb{R})\right)$ is an open set containing ξ^0 ; therefore, there exists a neighborhood V of ξ^0 included in $\mathfrak{J}^{-1}\left(GL_{2n}(\mathbb{R})\right)$. Finally, for any $\xi\in V$, $\mathcal{J}_k(\xi)=\mathfrak{J}(\xi)\in GL_{2n}(\mathbb{R})$, and hence, in

that neighborhood V, the descriptor system (37) takes the form of the nonlinear dynamical system

$$\dot{\xi} = \mathcal{J}_k(\xi)^{-1} A_k \gamma_k(\xi) \tag{38}$$

or, denoting by ϕ_k the mapping $\phi_k : \xi \mapsto \mathcal{J}_k(\xi)^{-1} A_k \gamma_k(\xi)$,

$$\dot{\xi} = \phi_k(\xi). \tag{39}$$

Before calculating the Jacobian of ϕ_k at ξ^0 in order to apply Lyapunov's indirect method, we introduce the following matrix:

$$\Gamma_k = D\mathcal{J}_k(\xi) = \frac{\partial \operatorname{vec} \mathcal{J}_k}{\partial \xi}.$$
 (40)

We have (we drop the dependencies on ξ when there is no ambiguity):

$$d\phi_k = d[\mathcal{J}_k(\xi)^{-1} A_k \gamma_k(\xi)] \tag{41}$$

$$= d\mathcal{J}_k(\xi)^{-1} A_k \gamma_k + \mathcal{J}_k^{-1} A_k d\gamma_k(\xi). \tag{42}$$

Then

$$d\mathcal{J}_k(\xi)^{-1} A_k \gamma_k = \text{vec} \left[d\mathcal{J}_k(\xi)^{-1} A_k \gamma_k \right]$$
 (43)

$$= (\gamma_k^T A_k^T \otimes I_{2n_k}) \operatorname{vec} d\mathcal{J}_k(\xi)^{-1}$$
 (44)

and by (148)

$$\operatorname{vec} d\mathcal{J}_k(\xi)^{-1} = \operatorname{vec} \left[-\mathcal{J}_k^{-1} d\mathcal{J}_k(\xi) \mathcal{J}_k^{-1} \right] \tag{45}$$

$$= - \left(\mathcal{J}_k^{-T} \otimes \mathcal{J}_k^{-1} \right) \operatorname{vec} d\mathcal{J}_k(\xi) \quad (46)$$

$$= -\left(\mathcal{J}_k^{-T} \otimes \mathcal{J}_k^{-1}\right) \Gamma_k d\xi. \tag{47}$$

We also have

$$d\gamma_k(\xi) = \mathcal{J}_k d\xi. \tag{48}$$

Plugging (44), (47), and (48) into (42) yields

$$d\phi_k = \left[-\left(\gamma_k^T A_k^T \otimes I_{2n_k}\right) \left(\mathcal{J}_k^{-T} \otimes \mathcal{J}_k^{-1}\right) \Gamma_k + \mathcal{J}_k^{-1} A_k \mathcal{J}_k \right] d\xi. \tag{49}$$

Therefore, we get the expression of the Jacobian of ϕ_k :

$$\frac{\partial \phi_k}{\partial \xi} = -\left(\gamma_k^T A_k^T \otimes I_{2n_k}\right) \left(\mathcal{J}_k^{-T} \otimes \mathcal{J}_k^{-1}\right) \Gamma_k + \mathcal{J}_k^{-1} A_k \mathcal{J}_k.$$
(50)

At ξ^0 , we have $\gamma_k(\xi^0) = 0$, and (50) simplifies into

$$\left. \frac{\partial \phi_k}{\partial \xi} \right|_{\xi^0} = \mathcal{J}_k(\xi^0)^{-1} A_k \mathcal{J}_k(\xi^0) \tag{51}$$

which has the same eigenvalues as A_k . From Lyapunov's indirect method [19, Th. 1, p. 246], [22, Corollary 4.3, p. 166], we conclude that (39) is exponentially stable.

In the multitask case, we also analytically linearize the system in the (q,\dot{q}) state space. In what follows, we require that the tasks together span the state space of the system, i.e., more formally that the matrix $B(\xi)$ in (52) is always positive definite. One practical way to ensure this condition is that at least one of the tasks k_0 is a full-configuration task $\tau_{k_0}(q)=q$, no matter how infinitesimally small its weight w_{k_0} is, as long as it remains positive $w_{k_0}>0$. This is a nonrestrictive assumption following the analysis in Section III-B.

Lemma 2: If one of the tasks is a full-configuration task, then, for all ξ , the matrix

$$B(\xi) = \sum_{k=1}^{p} w_k \mathcal{J}_k(\xi)^T \mathcal{J}_k(\xi)$$
 (52)

is nonsingular.

Proof: $B(\xi)$ is clearly a symmetric positive matrix. Since one of the tasks τ_{k_0} is a full-configuration task $\tau_{k_0}(q) = q$, we have $J_{k_0}(q) = I_n$, and from (35), $\mathcal{J}_{k_0}(\xi) = I_{2n}$; therefore

$$B(\xi) = w_{k_0} I_{2n} + \sum_{\substack{k=1\\k \neq k_0}}^{p} w_k \mathcal{J}_k(\xi)^T \mathcal{J}_k(\xi).$$
 (53)

Since $w_{k_0} > 0$, $B(\xi)$ is positive definite and thus nonsingular.

Proposition 4: Let us suppose $B(\xi) > 0$ (e.g., under the conditions of Lemma 2). The system

$$\dot{\xi} = \arg\min \sum_{k=1}^{p} w_k ||\dot{\eta}_k - A_k \eta_k||^2$$
 (54)

has an equilibrium if and only if there exists ξ^0 such that

$$\sum_{k=1}^{p} w_k \mathcal{J}_k(\xi^0)^T A_k \gamma_k(\xi^0) = 0.$$
 (55)

In that case, the equilibrium is exponentially stable if and only if the matrix

$$B^{-1} \sum_{k=1}^{p} w_k \left(\left(\gamma_k^T A_k^T \otimes I_{2n_k} \right) K_{2n_k 2n} \Gamma_k + \mathcal{J}_k^T A_k \mathcal{J}_k \right)$$
 (56)

evaluated at ξ^0 is stable.

Proof: The first-order optimality condition for (54) is

$$\frac{\partial}{\partial \dot{\xi}} \left[\sum_{k=1}^{p} w_k ||\dot{\eta}_k - A_k \eta_k||^2 \right] = 0 \tag{57}$$

$$\Leftrightarrow \sum_{k=1}^{p} 2 w_k \mathcal{J}_k^T (\dot{\eta}_k - A_k \eta_k) = 0$$
 (58)

$$\Leftrightarrow \left[\sum_{k=1}^{p} w_k \mathcal{J}_k^T \mathcal{J}_k\right] \dot{\xi} = \sum_{k=1}^{p} w_k \mathcal{J}_k^T A_k \eta_k.$$
 (59)

With $B(\xi)$ being nonsingular, (59) takes the form of the nonlinear system

$$\dot{\xi} = B(\xi)^{-1} \sum_{k=1}^{p} w_k \mathcal{J}_k(\xi)^T A_k \gamma_k(\xi)$$
 (60)

which admits an equilibrium if and only if there exists ξ^0 such that

$$\sum_{k=1}^{p} w_k \mathcal{J}_k(\xi^0)^T A_k \gamma_k(\xi^0) = 0.$$
 (61)

Let us linearize (60) around such an equilibrium. To do this, we calculate the Jacobian of the mapping $\psi: \xi \mapsto B(\xi)^{-1} \sum_{k=1}^p w_k \mathcal{J}_k(\xi)^T A_k \gamma_k(\xi)$ using the differential-based

treatment introduced in the Appendix. We have (dropping again the dependencies on ξ when appropriate)

$$d\psi = dB(\xi)^{-1} \sum_{k=1}^{p} w_k \mathcal{J}_k^T A_k \gamma_k$$

$$+ B^{-1} \sum_{k=1}^{p} w_k \left[d\mathcal{J}_k(\xi)^T A_k \gamma_k + \mathcal{J}_k^T A_k d\gamma_k(\xi) \right].$$
(62)

Let us calculate each term of the right-hand side of (62) separately. To shorten the expressions, let C denote the vector $C(\xi) = \sum_{k=1}^{p} w_k \mathcal{J}_k(\xi)^T A_k \gamma_k(\xi)$. We have, by (148),

$$dB(\xi)^{-1}C = -B^{-1}dB(\xi)B^{-1}C \tag{63}$$

$$= \operatorname{vec} \left[-B^{-1} dB(\xi) B^{-1} C \right]$$
 (64)

$$= -(C^T B^{-T} \otimes B^{-1}) \operatorname{vec} dB(\xi)$$
 (65)

where

$$\operatorname{vec} dB(\xi) = d\operatorname{vec} B(\xi) \tag{66}$$

$$= \sum_{k=1}^{p} w_k d \operatorname{vec} \mathcal{J}_{k}(\xi)^{\mathrm{T}} \mathcal{J}_{k}(\xi)$$
 (67)

and by (150)

$$d \operatorname{vec} \mathcal{J}_{k}^{T} \mathcal{J}_{k} = \left(I_{4n_{k}^{2}} + K_{2n_{k}2n_{k}} \right) \left(\mathcal{J}_{k} \otimes I_{2n_{k}} \right) \operatorname{d} \operatorname{vec} \mathcal{J}_{k}$$
 (68)

with

$$d \operatorname{vec} \mathcal{J}_{k}(\xi) = \Gamma_{k} d\xi. \tag{69}$$

This gives us the first term in (62) as

$$dB(\xi)^{-1}C = -\left(C^T B^{-T} \otimes B^{-1}\right) \sum_{k=1}^{p} w_k \left(I_{4n_k^2} + K_{2n_k 2n_k}\right) \left(\mathcal{J}_k \otimes I_{2n_k}\right) \Gamma_k d\xi.$$
 (70)

As for the other two terms, we write, applying (149) for (73)

$$d\mathcal{J}_k(\xi)^T A_k \gamma_k = \text{vec} \left[d\mathcal{J}_k(\xi)^T A_k \gamma_k \right]$$
 (71)

$$= \left(\gamma_k^T A_k^T \otimes I_{2n_k} \right) \operatorname{vec} d\mathcal{J}_k(\xi)^T \tag{72}$$

$$= \left(\gamma_k^T A_k^T \otimes I_{2n_k}\right) K_{2n_k 2n} \operatorname{vec} d\mathcal{J}_{\mathbf{k}}(\xi) \quad (73)$$

$$= \left(\gamma_k^T A_k^T \otimes I_{2n_k}\right) K_{2n_k 2n} \Gamma_k d\xi \tag{74}$$

and, finally, the last term

$$\mathcal{J}_k^T A_k d\gamma_k(\xi) = \mathcal{J}_k^T A_k \mathcal{J}_k d\xi. \tag{75}$$

Plugging (70), (74), and (75) into (62) gives us

$$d\psi = \left[-\left(C^T B^{-T} \otimes B^{-1} \right) \sum_{k=1}^p w_k \left(I_{4n_k^2} + K_{2n_k 2n_k} \right) \right]$$

$$\times (\mathcal{J}_k \otimes I_{2n_k})\Gamma_k + B^{-1} \sum_{k=1}^p w_k \Big((\gamma_k^T A_k^T \otimes I_{2n_k}) K_{2n_k 2n} \Gamma_k \Big)$$

$$+ \left[\mathcal{J}_k^T A_k \mathcal{J}_k \right] d\xi \tag{76}$$

from which we get the desired analytic expression of the Jacobian of the mapping ψ :

$$\frac{\partial \psi}{\partial \xi} = -\left(C^T B^{-T} \otimes B^{-1}\right) \sum_{k=1}^p w_k \left(I_{4n_k^2} + K_{2n_k 2n_k}\right)$$

$$\left(\mathcal{J}_k \otimes I_{2n_k}\right) \Gamma_k + B^{-1} \sum_{k=1}^p w_k \bigg(\big(\gamma_k^T A_k^T \otimes I_{2n_k} \big) K_{2n_k 2n} \Gamma_k$$

$$+ \mathcal{J}_k^T A_k \mathcal{J}_k$$
 (77)

At the equilibrium ξ^0 , we have from (61) $C(\xi^0) = 0$; hence, (77) simplifies into

$$\frac{\partial \psi}{\partial \xi} \Big|_{\xi^0} = B^{-1} \sum_{k=1}^p w_k \left(\left(\gamma_k^T A_k^T \otimes I_{2n_k} \right) K_{2n_k 2n} \Gamma_k + \mathcal{J}_k^T A_k \mathcal{J}_k \right).$$
(78)

Thus, the equilibrium ξ^0 is exponentially stable if and only if this latter matrix is stable.

Corollary 4: If the tasks τ_k are ultimately realizable simultaneously, i.e., if there exists ξ^0 such that $\forall k \in \{1,\ldots,p\}$ $\gamma_k(\xi^0) = 0$, then ξ^0 is an equilibrium of (54). In that case, a sufficient condition for ξ^0 to be exponentially stable is that the matrices $A_k + A_k^T$ are negative definite.

Proof: If $\forall k \in \{1, ..., p\}$, $\gamma_k(\xi^0) = 0$, then (55) holds, and by Proposition 4, ξ^0 is an equilibrium point of (54). Moreover, in that case, (56) simplifies into

$$\left[\sum_{k=1}^{p} w_k \mathcal{J}_k^T \mathcal{J}_k\right]^{-1} \sum_{k=1}^{p} w_k \mathcal{J}_k^T A_k \mathcal{J}_k = B^{-1} \mathcal{A}$$
 (79)

where we denoted

$$\mathcal{A} = \sum_{k=1}^{p} w_k \mathcal{J}_k^T A_k \mathcal{J}_k. \tag{80}$$

If we additionally suppose that $A_k + A_k^T$ are negative definite, then $\mathcal{A} + \mathcal{A}^T$ is also negative definite since

$$\mathcal{A} + \mathcal{A}^{T} = w_{k_0} \left(A_{k_0} + A_{k_0}^{T} \right) + \sum_{\substack{k=1\\k \neq k_0}}^{p} w_k \mathcal{J}_k^{T} \left(A_k + A_k^{T} \right) \mathcal{J}_k$$
(81)

with $w_{k_0} \left(A_{k_0} + A_{k_0}^T \right)$ negative definite (since $w_{k_0} > 0$) and $\forall k \neq k_0 \ w_k \mathcal{J}_k^T \left(A_k + A_k^T \right) \mathcal{J}_k$ negative.

Furthermore, with B being positive definite, $\mathcal{B}=B^{-1}$ is also symmetric positive definite. Any matrix congruent to a negative-definite matrix is also a negative-definite matrix, and hence, $\mathcal{B}\left(\mathcal{A}^T+\mathcal{A}\right)\mathcal{B}^T$ is negative definite. And given that

$$\mathcal{B}\left(\mathcal{A}^{T}+\mathcal{A}\right)\mathcal{B}^{T}=\mathcal{B}\left(\mathcal{A}^{T}+\mathcal{A}\right)\mathcal{B},\quad\left(\mathcal{B}\text{ symmetric}\right)$$
 (82)

$$= \mathcal{B} \mathcal{A}^T \mathcal{B} + \mathcal{B} \mathcal{A} \mathcal{B} \tag{83}$$

$$= \mathcal{B} \left(\mathcal{B} \mathcal{A} \right)^T + \left(\mathcal{B} \mathcal{A} \right) \mathcal{B} \tag{84}$$

then the pair of positive-definite matrices $Q = -\mathcal{B}(A^T + A)\mathcal{B}^T$ and $\mathcal{P} = \mathcal{B}$ satisfy the Lyapunov equation

 $\mathcal{P}(\mathcal{B}\mathcal{A})^T + (\mathcal{B}\mathcal{A})\mathcal{P} = -\mathcal{Q}$. Therefore, $\mathcal{B}\mathcal{A} = B^{-1}\mathcal{A}$ is stable. By Proposition 4, we conclude that ξ^0 is exponentially stable.

Remark 1: The terms $\left(\gamma_k^T A_k^T \otimes I_{2n_k}\right) K_{2n_k 2n} \Gamma_k$ can all be ignored in the expression of matrix (56) if and only if the tasks are all achievable simultaneously. When the tasks conflict and the equilibrium is a compromise between them, then these terms cannot be ignored and the full expression of (56) has to be considered for evaluating the stability of the system.

V. APPLICATION TO HUMANOID MULTITASK CONTROL

In this section, we determine the nature of the control decision variable x and characterize the constraint set \mathcal{X} in the humanoid control application case. We also cast the problem (29) as a linearly constrained QP inspired by approaches in the literature [33]–[37] (see the discussion at the end of Section V-C) and show some of its stability properties in the sense of existence, uniqueness, continuity, and robustness of its solution (that is, a "stability" sense different from the "Lyapunov stability" sense in Section IV).

A. Physical and Mathematical Constraints

Constraints of the humanoid robot motion include its equation of motion, the nonslipping contact constraints (e.g., at the feet surfaces), the corresponding Coulomb friction constraints, and various bounds on the applicable torques, admissible ranges of joint angles, joint velocities, and collision avoidance.

The equation of motion of a humanoid robot in a given contact phase is usually written as

$$M(q)\ddot{q} + N(q,\dot{q}) = Su + J^{c}(q)^{T}\lambda$$
(85)

$$J^{c}(q)\ddot{q} + \dot{J}^{c}(q)\dot{q} = 0.$$
 (86)

One additional constraint has to be appended to the system (85), (86) and yet is often omitted in many existing treatments of the problem, that is, the Coulomb friction cone constraint which then results into the following system:

$$M(q)\ddot{q} + N(q, \dot{q}) = Su + J^{c}(q)^{T}\lambda \tag{87}$$

$$J^c(q)\ddot{q} + \dot{J}^c(q)\dot{q} = 0 \tag{88}$$

$$\lambda \in \mathcal{C}$$
 (89)

with ${\mathcal C}$ denoting a Coulomb friction cone. Note that constraint (88) cannot be derived from any arbitrary holonomic constraint h(q)=0 that expresses the fixation of the contact (with $\frac{\partial\,h}{\partial\,q}=J^c$). For example, for any such constraint h(q)=0, the constraint $\|h(q)\|^2=0$ would mathematically express the exact same constraint but would result in a different Jacobian and thus in Lagrange multipliers that would not satisfy the same mathematical relations.

In order for the constraint (89) to physically make sense, λ has to be the actual physical contact forces, not arbitrary constraint forces. For a point contact at a point a belonging to a planar surface S of the robot with normal ν_S , the physical contact force λ is associated with the constraint $J^a\dot{q}=0$, where J^a is the Jacobian such that $\dot{a}=J^a\dot{q}$. In that case, the Coulomb friction cone takes the following form:

$$\mathcal{C}_{8} = \left\{ \lambda \in \mathbb{R}^{3} \mid \langle \lambda, \nu_{8} \rangle > 0, \|\lambda - \langle \lambda, \nu_{8} \rangle \nu_{8} \| \right.$$

$$\leq \mu \langle \lambda, \nu_{8} \rangle \right\}. \tag{90}$$

For distributed surface contact on a surface S, we would have a *continuum* of forces and likewise constraints in a system of the form:

$$M(q)\ddot{q} + N(q,\dot{q}) = Su + \iint_{a \in \mathbb{S}} J^a(q)^T \lambda(a) dS(a)$$
 (91)

$$\forall a \in S \quad J^a(q)\ddot{q} + \dot{J}^a(q)\dot{q} = 0 \tag{92}$$

$$\forall a \in \mathcal{S} \quad \lambda(a) \in \mathcal{C}_{\mathcal{S}}. \tag{93}$$

This system can, however, be simplified according to the following theorem.

Theorem 8 (see [38, Proposition 1]): If S is a convex polygon

$$S = \left\{ \sum_{i=1}^{s} \alpha_i a_i \mid \sum_{i=1}^{s} \alpha_i = 1 \right\}$$
 (94)

then we have the following equivalence:

$$\forall F \in \mathbb{R}^n : \exists \lambda : \mathbb{S} \to \mathcal{C}_{\mathbb{S}} \text{ s.t. } F = \iint_{a \in \mathbb{S}} J^a(q)^T \lambda(a) d\mathbb{S}(a)$$

 \Leftrightarrow

$$\exists (\lambda_1, \dots, \lambda_s) \in [\mathcal{C}_{\mathcal{S}}]^s \text{ s.t. } F = \sum_{i=1}^s J^{a_i}(q)^T \lambda_i.$$
 (95)

Additionally, if we stay under the conditions of Theorem 8, it is clear that

$$(92) \Leftrightarrow \forall i \in \{1, \dots, s\} \ J^{a_i}(q)\ddot{q} + \dot{J}^{a_i}(q)\dot{q} = 0$$
 (96)

$$\Leftrightarrow \qquad J^{\$}(q)\ddot{q} + \dot{J}^{\$}\dot{q} = 0 \tag{97}$$

where $J^{\mathbb{S}}$ denotes the rotational and translational Jacobian of any frame rigidly attached to \mathbb{S} . This latter remark together with Theorem 8 allows us to rewrite the continuum system of equations (91)–(93) in the following equivalent finite system form:

$$M(q)\ddot{q} + N(q,\dot{q}) = Su + \sum_{i=1}^{s} J^{a_i}(q)^T \lambda_i$$
 (98)

$$J^{\$}(q)\ddot{q} + \dot{J}^{\$}\dot{q} = 0 \tag{99}$$

$$\forall i \in \{1, \dots, s\} \quad \lambda_i \in \mathcal{C}_{\mathcal{S}}. \tag{100}$$

B. Structural Constraints

We write here the structural constraints using the weak componentwise order notation for vector inequalities as follows:

$$u_{\min} \le u \le u_{\max} \tag{101}$$

$$q_{\min} \le q \le q_{\max} \tag{102}$$

$$\dot{q}_{\min} \le \dot{q} \le \dot{q}_{\max} \tag{103}$$

and the collision avoidance between two bodies based on a velocity damper formulation

$$\dot{d} \ge -\kappa \frac{d - \delta_s}{\delta_i - \delta_c} \tag{104}$$

where d denotes the distance between the two bodies and δ_i , δ_s , and κ are an influence distance, a security distance, and a damping constant, respectively (see [39] for details on this particular formulation).

C. Casting the Problem as a QP

In order to cast the problem as a QP, we conservatively approximate the friction cone \mathcal{C}_8 with an inscribed polyhedral cone $\hat{\mathcal{C}}_8$ [40]. Let \mathcal{C} denote the matrix of the set of the polyhedral cone generators' coordinates in the world frame, and let c denote the number of generators, $\mathcal{C} \in \mathbb{R}^{3 \times c}$; then, we have $\lambda \in \hat{\mathcal{C}}_8$ if and only if $\exists \hat{\lambda} \in \mathbb{R}^c$, s.t. $\lambda = \mathcal{C}\hat{\lambda}$. The system (98)–(100) becomes

$$M(q)\ddot{q} + N(q,\dot{q}) = Su + \sum_{i=1}^{s} J^{a_i}(q)^T \mathcal{C}\hat{\lambda}_i$$
 (105)

$$J^{\mathcal{S}}(q)\ddot{q} + \dot{J}^{\mathcal{S}}\dot{q} = 0 \tag{106}$$

$$\forall i \in \{1, \dots, s\} \quad 0 \le \hat{\lambda}_i. \tag{107}$$

We also rewrite the constraints (101)–(104), respectively, as follows:

$$u_{\min} \le u \le u_{\max} \tag{108}$$

$$\frac{\dot{q}_{\min} - \dot{q}}{\Delta t} \le \ddot{q} \le \frac{\dot{q}_{\max} - \dot{q}}{\Delta t} \tag{109}$$

$$\frac{q_{\min} - q - \dot{q}\Delta t}{\frac{1}{2}\Delta t^2} \le \ddot{q} \le \frac{q_{\max} - q - \dot{q}\Delta t}{\frac{1}{2}\Delta t^2}$$
(110)

$$\ddot{d} \ge \frac{1}{\Delta t} \left(-\xi \frac{d - \delta_s}{\delta_i - \delta_s} - \dot{d} \right) \tag{111}$$

where Δt is a fixed parameter (e.g., control time step). Finally, we enforce the compactness of the feasible set by setting an arbitrarily large bound on $\hat{\lambda}$

$$\hat{\lambda} \leq \hat{\lambda}_{\text{max}}.$$
 (112)

It can now be seen that setting the control decision variable as $x=(\ddot{q},u,\hat{\lambda})\in\mathbb{R}^{2n-6+s\cdot c}$, the set of equations and inequalities (105)–(112) defining the feasible set $\mathcal{X}\subset\mathbb{R}^{2n-6+s\cdot c}$ are linear in x, i.e., \mathcal{X} is a an intersection of closed halfspaces. Let $H_ex=b_e$ denote the set of equations (105) and (106) and $H_ix\leq b_i$ denote the set of inequalities (107)–(112)

$$\mathcal{X} = \left\{ x = (\ddot{q}, u, \hat{\lambda}) \in \mathbb{R}^{2n - 6 + s \cdot c} \mid (105) \text{ to } (112) \right\}$$
 (113)

$$= \{ x \in \mathbb{R}^{2n - 6 + s \cdot c} \mid H_e x = b_e, H_i x \le b_i \}. \tag{114}$$

Denoting the matrix

$$K(q) = \left(J^{a_1}(q)^T \mathcal{C} \cdots J^{a_s}(q)^T \mathcal{C}\right) \in \mathbb{R}^{n \times s \cdot c}$$
 (115)

we have, in particular,

$$H_e = \begin{pmatrix} M(q) - K(q) - S \\ J^{\$}(q) & 0 & 0 \end{pmatrix}, b_e = \begin{pmatrix} -N(q, \dot{q}) \\ -\dot{J}^{\$}\dot{q} \end{pmatrix}. \quad (116)$$

To the set of tasks τ_1, \ldots, τ_p , of which we recall that the task τ_{k_0} is a full-configuration task $\tau_{k_0} = g_{k_0}(q) = q$, we append two additional components in the vector optimization problem (24)

$$\min_{x \in \mathcal{X}} f(x) = (\|\ddot{\tau}_1 - \ddot{\tau}_1^d\|^2, \dots, \|\ddot{\tau}_p - \ddot{\tau}_p^d\|^2, \|u\|^2, \|\hat{\lambda}\|^2).$$
(117)

We show now that the conditions of Theorem 6 hold. We shall invoke the following two theorems, reusing the notations of Section III.

Theorem 9 (see [18, Proposition 2.1.22, p. 15]): A sufficient condition for the \mathbb{R}^p_{\geq} -convexity of $\mathcal{Y} = f(\mathcal{X})$ is that \mathcal{X} is convex and the functions f_1, \ldots, f_n are convex.

convex and the functions f_1, \ldots, f_p are convex. Theorem 10 (see [18, Lemma 3.2.3, p. 52]): Let Y^+ denote the extended recession cone of a set Y, defined as

$$Y^{+} = \left\{ y' \mid \exists (\beta^{k}) \in \mathbb{R}^{\mathbb{N}}, \ \exists (y^{k}) \in Y^{\mathbb{N}}, \ \beta^{k} > 0, \right.$$

$$\text{s.t. } \beta^{k} \xrightarrow[k \to +\infty]{} 0, \ \beta^{k} y^{k} \xrightarrow[k \to +\infty]{} y' \right\}. \tag{118}$$

Let Y_1 and Y_2 be two nonempty closed sets. If

$$Y_1^+ \cap (-Y_2^+) = \{0\} \tag{119}$$

then $Y_1 + Y_2$ is closed.

We can now prove the following.

Proposition 5: if \mathcal{X} is nonempty, then the conditions of Theorem 6 hold for the problem (117).

Proof: We recall that in, finite dimension, compactness is equivalent to simultaneous closedness and boundedness. Since $\mathcal X$ is closed as the intersection of a finite number of closed halfspaces, and $\mathcal X$ is bounded by the constraints (107)–(109) and (112), $\mathcal X$ is compact. f in (117) being continuous, $\mathcal Y=f(\mathcal X)$ is, therefore, compact, which implies that it is closed and bounded.

The extended recession cone of a bounded set is $\{0\}$ by [18, Lemma 3.2.1 p. 52]; thus, $\mathcal{Y}^+ = \{0\}$, and hence, $\mathcal{Y}^+ \cap (-\mathbb{R}^{(p+2)+}_{\geq}) = \{0\}$. Since \mathcal{Y} and \mathbb{R}^p_{\geq} are closed, by Theorem 10, $\mathcal{Y} + \mathbb{R}^{p+2}_{\geq}$ is closed, i.e., \mathcal{Y} is \mathbb{R}^{p+2}_{\geq} -closed.

Moreover, \mathcal{X} is convex as the intersection of a finite number of closed halfspaces, which are convex sets, and the functions f_1, \ldots, f_{p+2} in (117) are convex; then, by Theorem 9, \mathcal{Y} is \mathbb{R}^{p+2}_{\geq} -convex.

With Proposition 5, we can now safely consider the weightedsum scalarization of (117) with strictly positive weights 0 < wwithout sacrificing the completeness of all the achievable task behaviors

$$\min_{x \in \mathcal{X}} \sum_{k=1}^{p} w_k \| \ddot{\tau}_k - \ddot{\tau}_k^d \|^2 + w_{p+1} \| u \|^2 + w_{p+2} \| \hat{\lambda} \|^2.$$
 (120)

Problem (120) is a QP of the form

$$\min_{x} x^{T} Q x + l^{T} x$$
subject to $H_{e} x = b_{e}, H_{i} x \leq b_{i}$

$$(121)$$

where, in particular,

$$Q = \begin{pmatrix} \sum_{k=1}^{p} w_k J_k^T J_k & 0 & 0\\ 0 & w_{p+1} I_{n-6} & 0\\ 0 & 0 & w_{p+2} I_{s \cdot c} \end{pmatrix}.$$
(122)

Different variants of the formulation (120) and (121) were originally derived in the literature, e.g., [33, eq. (5)], [34, Fig. 4 and eq. (16)], [36, eq. (20)], [37, eq. (20)]. All these formulations can be seen as somewhat equivalent, with the later ones incorporating additional structural constraints and features (e.g. joint and velocity limits) that were absent from earlier ones, hence gradually becoming more complete and physically consistent. Other differences between the various weighted multitask QPs in the literature lie in the choice of the particular tasks or objectives, with, for example, [35, eq. (13)] incorporating an angular



Fig. 1. Example experiment with the HRP-4 humanoid robot.

momentum objective to control the center of pressure position (although it uses a less accurate, penalty-based rather than constraint-based, contact model). However, all these formulations can be fit in the general framework of (120) with, as such, differences in the particular formulation of the $\mathcal X$ constraint set and in the choices of the $\|\ddot{\tau}_k - \ddot{\tau}_k^d\|^2$ tasks.

The humanoid multiobjective QP formulation was later applied (or based upon) in the control architectures of different humanoid robots. [41, QP 5.1] used it in a control architecture for the HRP-2 robot. Many of the Atlas robot teams in the DARPA Robotics Challenge (2015) designed their control architectures based on a multiobjective QP formulation [42]. The WPI-CMU team used an equivalent formulation to the one we presented here [43, eq. (1) and Sec. 5]. The IHMC team used a reduced and faster formulation with only centroidal dynamics rather than full-body dynamics (at the expense of not accounting for torque limits), and they also wrote the motion objectives as joint acceleration constraints [44, Fig. 1 and eq. (21)]. Finally, the MIT team used a different formulation, which does not fit in the formulation (120), incorporating LQR-based CoM trajectory optimization directly in the QP, as an additional cost function objective along with the objectives considered here [45, Fig. 6 and QP 1]. However, their formulation was also inspired by the classical framework analyzed here (see the discussion in [45, Sec. 4.4]).

D. Stability of the QP

To conclude this section, we study some stability properties of the QP (121). Note that the notion of "stability" we consider here is different from the one in Section IV, as we understand the term "stability" of the QP in the sense of 1) existence and uniqueness of a solution (see Propositions 6 and 9); 2) robustness of the solution with respect to problem perturbations (see Lemma 3 and Propositions 7–9); and 3) continuity of the solution of the QP with respect to its parameters (see Corollary 5 and Proposition 9). This is the notion of stability we study here, which is complementary to the one studied in Section IV. Related work for a different control approach can be found, for example, in [32]. We are interested in the questions of existence, uniqueness, and continuity of the solution, as well as robustness to perturbations and modeling uncertainties. We will take as a first assumption the nonemptiness of \mathcal{X} (i.e., the feasibility of the problem) at a given initial state ξ^0 . Other assumptions we will make is the full row rank condition of the matrix H_e in (116), i.e., rank $H_e = n + 6$, and the *regularity* of the system

$$H_e x = b_e, \ H_i x \le b_i. \tag{123}$$

Definition 9 (see [46, Definition, p. 755], [47, Definition, p. 512]): The system of equations and inequalities (123) is said to be regular if H_e has full row rank and there exists x such that $H_e x = b_e$ and $H_i x < b_i$.

Lemma 3: Q is symmetric positive definite. Moreover, for any perturbation resulting from the updating of the state (q,\dot{q}) or from uncertainty in the model, the perturbed matrix $Q + \delta Q$ remains positive definite.

Proof: Isolating the configuration task τ_{k_0} in (122), we obtain

$$Q = \begin{pmatrix} w_{k_0} I_n & 0 & 0\\ 0 & w_{p+1} I_{n-6} & 0\\ 0 & 0 & w_{p+2} I_{s \cdot c} \end{pmatrix} + \sum_{\substack{k=1\\k \neq k_0}}^{p} \begin{pmatrix} w_k J_k^T J_k & 0 & 0\\ 0 & 0 & 0\\ 0 & 0 & 0 \end{pmatrix}.$$
(124)

Since 0 < w, we have in particular w_{k_0} , w_{p+1} , $w_{p+2} > 0$, and therefore, Q is symmetric positive definite. The perturbations of the state and the model would affect only J_k for $k \neq k_0$ on the right-hand side of (124), with $(J_k + \delta J_k)^T (J_k + \delta J_k)$ remaining positive, and therefore, $Q + \delta Q$ remains positive definite.

Remark 2: We can also show that Q>0 from the less strong assumption of B>0. Indeed, B>0 implies that $\sum_k w_k J_k^T J_k > 0$ (\mathcal{J}_k being block triangular with both block diagonal terms being equal to J_k). This assumption amounts to the set of tasks spanning the joint space without necessarily requiring that one of the tasks is a full-configuration task.

Proposition 6: If \mathcal{X} is nonempty, then (121) reaches a minimum at a unique point, i.e., the solution exists and is unique.

Proof: The set \mathcal{X} being compact and the mapping $\mathfrak{F}: x \mapsto x^T Q x + l^T x$ being continuous, from the extreme value theorem, (121) has a minimum. \mathfrak{F} being strictly convex from Q positive definite by Lemma 3, the minimizer is unique.

Proposition 7: A sufficient condition for the full row rank condition of H_e is that rank (K(q) S) = n (i.e., the contact forces completely make up for the underactuation).

Proof: Let L(q) = (-K(q) - S). We have

$$n+6 \ge \operatorname{rank} H_e = \operatorname{rank} \begin{pmatrix} M(q) \ L(q) \\ J^{8}(q) \ 0 \end{pmatrix}$$
 (125)

$$\geq \operatorname{rank} L(q) + \operatorname{rank} J^{8}(q)$$
 (126)

$$= \operatorname{rank} L(q) + 6. \tag{127}$$

Therefore, rank $H_e = n + 6$ if rank L(q) = n.

Proposition 8: Let x^0 denote the solution of (121) at an initial point ξ^0 . If the system (123) is regular, then there exists $\epsilon_1>0$ and $\mathcal{K}_1>0$ such that, for any update of the state ξ or modeling error (in particular, in $M(q), N(q,\dot{q})$, and the various Jacobians of the robot), the perturbed system

$$(H_e + \delta H_e)x = b_e + \delta b_e, (H_i + \delta H_i)x \le b_i + \delta b_i$$
 (128)

remains solvable and regular for those perturbations $(\delta H_e, \delta H_i, \delta b_e, \delta b_i)$ such that

$$\left\| \begin{pmatrix} \delta H_e \\ \delta H_i \end{pmatrix} \right\| + \left\| \begin{pmatrix} \delta b_e \\ \delta b_i \end{pmatrix} \right\| \le \epsilon_1 \tag{129}$$

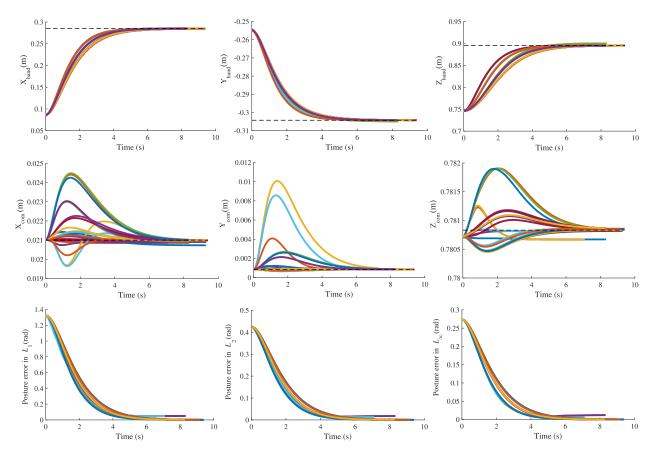


Fig. 2. Tasks and state convergence when varying weights. We plot the trajectories for 27 runs of the hand reaching experiment on the HRP-4 robot with different sets of weights to assess the results from Corollary 2 and Proposition 2 ($3 \times 3 \times 3$ values of $(w_{\text{hand}}, w_{\text{com}}, w_q) \in \{10^{-1}, 10^2, 10^3\}^3$). As predicted by Corollary 2, although the tasks do not necessarily always converge to zero (e.g., two runs do not yield a zero-converging Z_{com} and X_{com} error and two runs do not yield a zero-converging posture error), yet there exists always a set of weights such that the acceleration error of the task is below any given precision ϵ , which in turn ensures the boundedness of the error or the convergence to zero of the error of the task by Proposition 2. The trajectories also illustrate the results from Section V (see Propositions 6–9 and Corollary 5) as the QP controller outputs a continuous solution.

(130)

and, denoting x any solution of (128) with $\delta x = x - x^0$, we have

$$\begin{split} &\|\delta x\| \leq \\ &\mathcal{K}_1\left(\left|\left|\left(\frac{\delta H_e}{\delta H_i}\right)\right|\right| + \left|\left|\left(\frac{\delta b_e}{\delta b_i}\right)\right|\right|\right) \max\{1,\|x^0\|\}(1+\|x^0\|). \end{split}$$

Proof: This is a direct application of [47, Corollary 7] since the conditions of the latter corollary are all satisfied in the present case. [47, Corollary 7] is itself a direct consequence of the original work of Robinson [46, Th. 1]. See also the discussion in [48] and [49].

Proposition 9: Let $p=(\delta Q,\delta l,\delta H_e,\delta H_i,\delta b_e,\delta b_i)$ denote a perturbation of the QP (121). We suppose that H_e and $H_e+\delta H_e$ are both full row rank and that the system (123) is regular at the initial state ξ^0 . Then, there exists $\epsilon_2>0$ and $\mathcal{K}_2>0$ such that the solution $x^*=x^0+\delta x$ of the perturbed QP

$$\min_{x} x^{T} (Q + \delta Q)x + (l + \delta l)^{T} x$$

subject to $(H_e + \delta H_e)x = b_e + \delta b_e, (H_i + \delta H_i)x \leq b_i + \delta b_i$ (131)

exists and is unique and satisfies, whenever $||p||_{\infty} < \epsilon_2$

$$||x^* - x^0|| < \mathcal{K}_2 ||p||_{\infty}.$$
 (132)

Proof: Our aim here is to apply [50, Th. 4.4]. We thus shall show that the hypotheses [50, eqs. (3.1)–(3.4)] hold. First, we know that the conditions of Proposition 8 hold; thus, the first conclusion we can draw from that Proposition is that there exists $\epsilon_1 > 0$ such that the system (128) is regular and solvable whenever (129) hold. Hence, both feasible sets of (121) and (131) are nonempty under (129), which constitutes the first of the needed hypotheses. The other hypotheses are already satisfied by our assumptions, and therefore, we can apply [50, Th. 4.4], from which we deduce that, under (129), there exist $\epsilon_1' > 0$ and \mathcal{K}_2 such that if $\|p\|_{\infty} < \epsilon_1'$ and x' is any solution that minimizes (131), we have $\|x^0 - x'\| < \|p\|_{\infty}$. From Lemma 3, $Q + \delta Q$ is positive definite, and thus, x' is unique, and we denote it x^* . Take now

$$\epsilon_2 = \min\left\{\frac{\epsilon_1}{4}, \epsilon_1'\right\}. \tag{133}$$

We have

$$||p||_{\infty} < \epsilon_2 \quad \Rightarrow \quad (129) \text{ and } ||p||_{\infty} < \epsilon'_1.$$
 (134)

We, finally, conclude that if $||p||_{\infty} < \epsilon_2$, then $||x^* - x^0|| < \mathcal{K}_2 ||p||_{\infty}$.

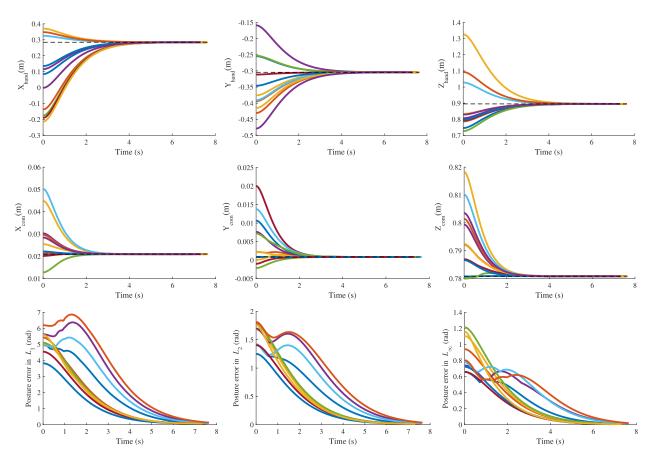


Fig. 3. Tasks and state convergence from random initial states to assess stability of the system (31) by Proposition 4. We plot the trajectories for ten runs of the hand reaching experiment of the HRP-4 robot starting from ten randomly sampled initial configurations in the upper body of the robot (randomly sampled joint angles of the upper-body joints) for a fixed set of weights $(w_{\text{hand}}, w_{\text{com}}, w_q) = (10^3, 10^3, 10^{-1})$. The errors converge to zero from any of these initial random configurations, which positively correlate to the stability of the matrices of Proposition 4, as shown in Figs. 5 and 6.

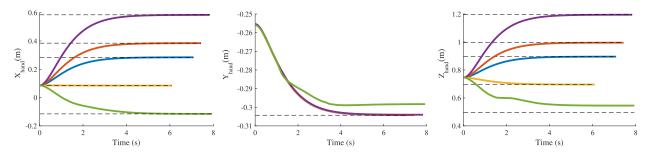


Fig. 4. Changing the task objective for the hand with a fixed set of weights $(w_{\text{hand}}, w_{\text{com}}, w_q) = (10^3, 10^3, 10^{-1})$. One of the positions was unachievable without compromising the equilibrium of the robot, which led to not realizing the task with that set of weights.

Corollary 5: In the context and with the notations of Proposition 9, the mapping $p \mapsto x^*$ is well defined on a neighborhood of 0 and continuous at 0.

Proof: Immediate from Proposition 9.

VI. EXPERIMENTAL VALIDATION

To illustrate our results, we applied the control scheme proposed in Section V to the humanoid robot HRP-4. The robot has to perform a whole-body reaching task with its right hand while keeping balance and sustaining feet contact with the ground (see

Fig. 1). The corresponding video and more complex experiments can be found online at the url given in [51].

We use the controller formulation (120), or in an equivalent form the QP controller (121). Propositions 6–9 and Corollary 5 are, hence, applicable, and as a result, the controller outputs a continuous solution, producing a smooth motion, as can be read in Figs. 2–4. We plot in these figures the feedforward command sent to the robot with task-level feedback.

The robot has 56 degrees of freedom, including the degrees of freedom of the hand fingers, i.e., n=56 and $q\in\mathbb{R}^{56}$. We define a set of p=3 tasks for the robot: a right-hand position task $\tau_{\text{hand}}\in\mathbb{R}^3$ to reach the desired workspace goal, a

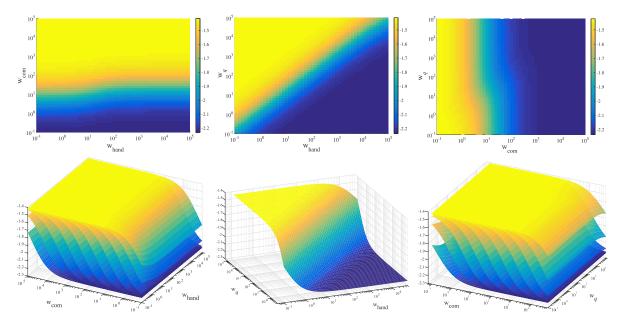


Fig. 5. Matrix stability from Proposition 4. We discretized the $(w_{\mathrm{hand}}, w_{\mathrm{com}}, w_q)$ space in $50 \times 50 \times 50$ grid in the logarithmic scale ranging from 10^{-1} to 10^5 along each dimension of the weight vector $(w_{\mathrm{hand}}, w_{\mathrm{com}}, w_q) \in \mathtt{logspace}(-1, 5, 50)^3$. We plot in color scale and surface plot the maximum real part of the eigenvalues of the matrix from Proposition 4. We see that this maximum is always negative; hence, the matrices are stable. In the top row figures, we plot the maximum real part of the eigenvalues along two dimensions of the weight vector for a given value of the third dimension (10^4) . In the bottom row figures, we plot the same data for ten values in $\mathtt{logspace}(-1, 5, 10)$ along the third dimension, while the other two dimensions are in $\mathtt{logspace}(-1, 5, 50)^2$, which result in ten surfaces in each plot (the ten surfaces are very close to each other in the middle column).

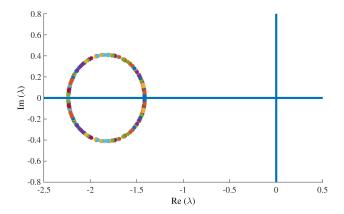


Fig. 6. All 112 000 eigenvalues (counting multiplicities) of the 112 \times 112 matrices from Proposition 4 for 1000 set of weights ranging in the logarithmic scale from 10^{-1} to 10^{5} , i.e., $(w_{\rm hand}, w_{\rm com}, w_q) \in {\tt logspace}(-1,5,10)^3$. All the eigenvalues are located in the left complex half plane, which means they are stable.

center-of-mass task $\tau_{\rm com} \in \mathbb{R}^3$ to keep equilibrium while performing the task, and a full-configuration task $\tau_q = q \in \mathbb{R}^{56}$ for stability and redundancy resolution, as required in Lemmas 2 and 3. For these three tasks, we design attractor behaviors (3) with matrices $P_{\rm hand} = k_{\rm hand}I_3$, $P_{\rm hand} = 2\sqrt{k_{\rm hand}}I_3$, $P_{\rm com} = k_{\rm com}I_3$, $P_{\rm com} = 2\sqrt{k_{\rm com}}I_3$, $P_q = k_qI_{56}$, $P_q = 2\sqrt{k_q}I_{56}$, and $(k_{\rm hand}, k_{\rm com}, k_q) = (2, 5, 5)$ (standard values we use in most of our control scenarios; these do not require any specific fine tuning). These matrices allow us to derive the matrices $A_{\rm hand}$, $A_{\rm com}$, and A_q , respectively. Fig. 2 shows the convergence behavior of the tasks along a subset of $3\times 3\times 3$ values of the weights as run on the robot HRP-4.

Using the MATLAB function logspace, we discretize the weight space $(w_{\text{hand}}, w_{\text{com}}, w_q)$ in a $50 \times 50 \times 50$ grid ranging

in a logarithmic scale from 10^{-1} to 10^{5} along each of the three dimensions, i.e., $(w_{\rm hand},w_{\rm com},w_q)\in {\tt logspace}(-1,5,50)^3$. We then compute the matrices

$$\mathbb{R}^{112 \times 112} \ni \Xi[w_{\text{hand}}, w_{\text{com}}, w_q]$$

$$= \left[\sum_{k \in \{\text{hand,com}, q\}} w_k \mathcal{J}_k^T \mathcal{J}_k \right]^{-1} \sum_{k \in \{\text{hand,com}, q\}} w_k \mathcal{J}_k^T A_k \mathcal{J}_k$$
(135)

which are the forms of the matrix (56) in Proposition 4 when the tasks are achievable (this is the case here as the tasks were planned with a planner and a posture generator). Since at the equilibrium ξ^0 we have $\dot{q}=0$, then the matrices \mathcal{J}_k take here the forms

$$\mathcal{J}_k(\xi^0) = \begin{pmatrix} J_k(q^0) & 0\\ 0 & J_k(q^0) \end{pmatrix}, k \in \{\text{hand}, \text{com}, q\}. \quad (136)$$

In order to evaluate the stability of the matrices Ξ , using the MATLAB function eig, we compute the eigenvalues of the matrices $\Xi[w_{\rm hand},w_{\rm com},w_q]$ that we plot in Fig. 6. We then compute the maximum real part of the eigenvalues of each of these matrices and plot them in Fig. 5. All the matrices are stable since their eigenvalues have all negative real parts. Hence, by Proposition 4, the equilibrium point of the system (31), which corresponds to the closed-loop dynamical system resulting from the unconstrained version of the multiobjective optimization, is exponentially stable, giving hints on the Lyapunov stability of the QP (120). Finally, this result is validated by running the controller starting from ten randomly sampled initial configurations in the upper body of the robot, as displayed in Fig. 3.

Note that on the limitations side, we experienced numerical instability issues when the range of weights was extended to a

ratio between the smallest and largest weight above 10^7 . This is due the real optimization problem running on floating-point hardware and becoming ill-conditioned when that ratio becomes too large and is an inherent limitation of the nonconstructive pure existence proofs of the results in Section III-B, more aimed toward theoretical foundation of the proposed multitask control approach.

VII. CONCLUSION

We have demonstrated that the essence of the multitask control problem can be effectively captured by the multiobjective optimization formal framework. We discussed the pertinence of scalarizing the vector optimization problem as a weighted sum with positive weights and proved that the positive-weight scalarization does indeed satisfy a completeness property with respect to all the efficient solutions, the popular lexicographic solution being one of them. We studied Lyapunov stability of the feedback system resulting from such a weighted-sum scalarization scheme in the unconstrained optimization case and proposed some necessary and/or sufficient conditions for the exponential stability of the equilibrium points of the systems. Finally, we applied the study to the particular case of the humanoid robot. We demonstrated that, in that case, the positive weightedsum scalarization leads to a linearly constrained positive-definite quadratic problem that is stable (in the robustness and solutionguaranteed sense) and well behaved under the stated regularity conditions.

Future work is dedicated to translating some of the non-constructive pure existence proofs of this paper, proposed essentially as theoretical foundation layers, into practical weight tuning algorithms, which constitutes an active topic of research. We are also planning to extend the Lyapunov stability analysis to the feedback dynamical system resulting from a constrained multiobjective optimization formulation, with both equality and inequality constraints. This is still an open problem, and the contributions of the present paper will be used as the primary building blocks for that follow-up work.

APPENDIX MATRIX DIFFERENTIATION TOOLS FOR LYAPUNOV'S INDIRECT METHOD

We introduce a tool to efficiently differentiate $J_k(q)$ with respect to q, which can somewhat be termed the "Jacobian of the Jacobian" (which is not to be confused with the notion of a *Hessian matrix* that is only defined for scalar functions). Unfortunately, the expression

$$\frac{\text{``}\partial J_k(q)}{\partial q}$$
 (137)

does not make sense and is not properly defined, since it involves the differentiation of a matrix with respect to a vector. Magnus and Neudecker proposed to use the following quantity that is thoroughly consistent with all the properties of the classical differentiation frameworks (in particular, with the chain rule, the notion of the Jacobian, and Cauchy's rule of invariance) [52]:

$$G_k = DJ_k(q) = \frac{\partial \operatorname{vec} J_k(q)}{\partial q}.$$
 (138)

The vec operator denotes the vectorization operator, which consists for a matrix in stacking its columns as a vector, i.e.,

$$\operatorname{vec}\begin{pmatrix} a_{11} & \cdots & a_{1m} \\ \vdots & \ddots & \vdots \\ a_{n1} & \cdots & a_{nm} \end{pmatrix} = \begin{pmatrix} a_{11} \\ \vdots \\ a_{n1} \\ \vdots \\ \vdots \\ a_{1m} \\ \vdots \\ a_{nm} \end{pmatrix}. \tag{139}$$

Definition 10 (see [53, Definition 3.1, p. 383]): There exists a so-called commutation matrix K_{nm} , that is the $nm \times nm$ permutation matrix, which transforms $\operatorname{vec} A^T$ into $\operatorname{vec} A$ for any $n \times m$ matrix A, i.e., $\forall A \in \mathbb{R}^{n \times m}$ $\operatorname{vec} A^T = K_{mn} \operatorname{vec} A$.

Denoting \otimes the *Kronecker product*, we have the following.

Theorem 11 (see [54, Proposition 7.1.9, p. 401 and Fact 7.4.6, p. 405]): For any vector X and matrices A, B, and C such that ABC is defined, we have

$$X = \operatorname{vec} X \tag{140}$$

$$\operatorname{vec}(ABC) = (C^T \otimes A)\operatorname{vec} B$$
 (141)

$$\operatorname{vec}(AB) = (I \otimes A)\operatorname{vec}B$$
 (142)

$$\operatorname{vec}(AB) = (B^T \otimes I)\operatorname{vec} A.$$
 (143)

Definition 11 (see [52, Definition 5, p. 479]): A matrix function $F: S \subset \mathbb{R}^{n \times m} \to \mathbb{R}^{p \times q}$ is differentiable at $C \in \text{int}(S)$ if there exists a matrix $A(C) \in \mathbb{R}^{mn \times pq}$ such that, for U in a neighborhood of 0 in $\mathbb{R}^{n \times m}$, we have

$$\text{vec } F(C + U) = \text{vec } F(C) + A(C)\text{vec } U + o(\|U\|).$$
 (144)

If A(C) exists, it is unique and the $p \times q$ matrix dF(C;U) defined by

$$\operatorname{vec} dF(C; U) = A(C)\operatorname{vec} U \tag{145}$$

is called the differential of F at C with increment U.

Theorem 12 (see [55, Th. 11, p. 108]): If F is differentiable at C, then A(C) defined in Definition 6 is the Jacobian of $\operatorname{vec} F$ with respect to $\operatorname{vec} X$ (X denoting the variable of F) that we also call the Jacobian of F at X

$$A(C) = DF(C) = \frac{\partial \operatorname{vec} F}{\partial \operatorname{vec} X} \Big|_{C}$$
 (146)

Theorem 13 (Cauchy's rule of invariance [55, Th. 13, p. 108]): If F is differentiable at C and G is differentiable at B = F(C), then $H = G \circ F$ is differentiable at C and

$$dH(C;U) = dG(B; dF(C;U)). \tag{147}$$

Example 1 (see [55, Th. 3, p. 71 and Ch. 9, Sec. 13, pp. 205–208]): The differentials of the mappings $GL_n(\mathbb{R}) \to \mathbb{R}^n$ $X \mapsto X^{-1}$; $\mathbb{R}^{n \times m} \to \mathbb{R}^{m \times n}$, $X \mapsto X^T$; and $\mathbb{R}^{n \times m} \to \mathbb{R}^{n \times n}$,

 $X \mapsto X^T X$ can be derived, respectively, as

$$d(X^{-1}) = -X^{-1}dXX^{-1} (148)$$

$$d(X^T) = K_{nm} dX (149)$$

$$d(X^T X) = (K_{mm} + I_{m^2}) (I_m \otimes X^T) dX. \quad (150)$$

Hence, by Cauchy's rule of invariance, we can write for $J_k(q)$ seen as a function of q:

$$dJ_k(q)^{-1} = -J_k^{-1} dJ_k(q) J_k^{-1}$$
 (J(q) nonsingular)

(151)

$$d(J_k(q)^T) = K_{n_k n} dJ_k(q)$$
(152)

$$d(J_k(q)^T J_k(q)) = \left(K_{n_k n_k} + I_{n_k^2}\right) \left(I_{n_k} \otimes J_k^T\right) dJ_k(q).$$
(153)

REFERENCES

- O. Khatib, "A unified approach for motion and force control of robot manipulators: The operational space formulation," *IEEE J. Robot. Autom.*, vol. RA-3, no. 1, pp. 43–53, Feb. 1987.
- [2] J. Nakanishi, R. Cory, M. Mistry, J. Peters, and S. Schaal, "Operational space control: A theoretical and empirical comparison," *Int. J. Robot. Res.*, vol. 27, no. 6, pp. 737–757, 2008.
- [3] L. Sentis, J. Park, and O. Khatib, "Compliant control of multicontact and center-of-mass behaviors in humanoid robots," *IEEE Trans. Robot.*, vol. 26, no. 3, pp. 483–501, Jun. 2010.
- [4] M. Mistry and L. Righetti, "Operational space control of constrained and underactuated systems," in *Proc. Robot.: Sci. Syst. Conf.*, Los Angeles, CA, USA, Jun. 2011.
- [5] L. Righetti, J. Buchli, M. Mistry, M. Kalakrishnan, and S. Schaal, "Optimal distribution of contact forces with inverse dynamics control," *Int. J. Robot. Res.*, vol. 32, no. 3, pp. 280–298, 2013.
- [6] L. Saab, O. Ramos, F. Keith, N. Mansard, P. Soueres, and J. Fourquet, "Dynamic whole-body motion generation under rigid contacts and other unilateral constraints," *IEEE Trans. Robot.*, vol. 29, no. 2, pp. 346–362, Apr. 2013.
- [7] C. Ott, A. Dietrich, and A. Albu-Schäffer, "Prioritized multi-task compliance control of redundant manipulators," *Automatica*, vol. 53, pp. 416–423, 2015.
- [8] N. Mansard and F. Chaumette, "Directional redundancy for robot control," IEEE Trans. Automat. Control, vol. 54, no. 6, pp. 1179–1192, Jun. 2009.
- [9] C.-Y. Su and Y. Stepanenko, "Adaptive variable structure set-point control of underactuated robots," *IEEE Trans. Automat. Control*, vol. 44, no. 11, pp. 2090–2093, Nov. 1999.
- [10] M. Reyhanoglu, A. van der Schaft, N. McClamroch, and I. Kolmanovsky, "Dynamics and control of a class of underactuated mechanical systems," *IEEE Trans. Automat. Control*, vol. 44, no. 9, pp. 1663–1671, Sep. 1999.
- [11] H. Kazerooni, "Contact instability of the direct drive robot when constrained by a rigid environment," *IEEE Trans. Automat. Control*, vol. 35, no. 6, pp. 710–714, Jun. 1990.
- [12] A. Ten Dam, K. Dwarshuis, and J. Willems, "The contact problem for linear continuous-time dynamical systems: A geometric approach," *IEEE Trans. Automat. Control*, vol. 42, no. 4, pp. 458–472, Apr. 1997.
- [13] J. Wen and S. Murphy, "Stability analysis of position and force control for robot arms," *IEEE Trans. Automat. Control*, vol. 36, no. 3, pp. 365–371, Mar. 1991.
- [14] B. Brogliato, "Some perspectives on the analysis and control of complementarity systems," *IEEE Trans. Automat. Control*, vol. 48, no. 6, pp. 918–935, Jun. 2003.
- [15] M. Spong, J. Thorp, and J. Kleinwaks, "The control of robot manipulators with bounded input," *IEEE Trans. Automat. Control*, vol. AC-31, no. 6, pp. 483–490, Jun. 1986.
- [16] K. Bouyarmane and A. Kheddar, "Humanoid robot locomotion and manipulation step planning," Adv. Robot., vol. 26, no. 10, pp. 1099–1126, 2012.
- [17] M. Ehrgott, Multicriteria Optimization. Berlin, Germany: Springer-Verlag, 2005.

- [18] Y. Sawaragi, H. Nakayama, and T. Tanino, Theory of Multiobjective Optimization. San Francisco, CA, USA: Academic, 1985.
- [19] M. Vidyasagar, Nonlinear Systems Analysis, 2nd ed. Philadelphia, PA, USA: SIAM, 2002.
- [20] M. Corless and G. Leitmann, "Continuous state feedback guaranteeing uniform ultimate boundedness for uncertain dynamic systems," *IEEE Trans. Automat. Control*, vol. AC-26, no. 5, pp. 1139–1144, Oct. 1981.
- [21] M. Spong, "On the robust control of robot manipulators," *IEEE Trans. Automat. Control*, vol. 37, no. 11, pp. 1782–1786, Nov. 1992.
- [22] H. Khalil, Nonlinear Systems. Englewood Cliffs, NJ, USA: Prentice-Hall, 2002.
- [23] G. Söderlind, "The logarithmic norm: History and modern theory," BIT Numer. Math., vol. 46, no. 3, pp. 631–652, 2006.
- [24] G. Dahlquist, "Stability and error bounds in the numerical integration of ordinary differential equations," Ph.D. dissertation, Roy. Inst. Technol., Stockholm, Sweden, 1958.
- [25] P. L. Yu, "Cone convexity, cone extreme points, and nondominated solutions in decision problems with multiobjectives," *J. Optim. Theory Appl.*, vol. 14, no. 3, pp. 319–377, 1974.
- [26] A. M. Geoffrion, "Proper efficiency and the theory of vector maximization," J. Math. Anal. Appl., vol. 22, no. 3, pp. 618–630, 1968.
- [27] R. Hartley, "On cone-efficiency, cone-convexity and cone-compactness," SIAM J. Appl. Math., vol. 34, no. 2, pp. 211–222, 1978.
- [28] A. Escande, N. Mansard, and P.-B. Wieber, "Hierarchical quadratic programming: Fast online humanoid-robot motion generation," *Int. J. Robot. Res.*, vol. 33, no. 7, pp. 1006–1028, 2014.
- [29] P. Chiacchio, S. Chiaverini, L. Sciavicco, and B. Siciliano, "Closed-loop inverse kinematics schemes for constrained redundant manipulators with task space augmentation and task priority strategy," *Int. J. Robot. Res.*, vol. 10, no. 4, pp. 410–425, 1991.
- [30] G. Antonelli, "Stability analysis for prioritized closed-loop inverse kinematic algorithms for redundant robotic systems," *IEEE Trans. Robot.*, vol. 25, no. 5, pp. 985–994, Oct. 2009.
- [31] A. Ames, K. Galloway, K. Sreenath, and J. Grizzle, "Rapidly exponentially stabilizing control Lyapunov functions and hybrid zero dynamics," *IEEE Trans. Automat. Control*, vol. 59, no. 4, pp. 876–891, Apr. 2014.
- [32] B. Morris, M. Powell, and A. Ames, "Sufficient conditions for the Lipschitz continuity of QP-based multi-objective control of humanoid robots," in *Proc. IEEE Annu. Conf. Decision Control*, Dec. 2013, pp. 2920–2926.
- [33] Y. Abe, M. da Silva, and J. Popović, "Multiobjective control with frictional contacts," in *Proc. ACM SIGGRAPH/Eurograph. Symp. Comput. Animation*, 2007, pp. 249–258.
- [34] C. Collette, A. Micaelli, C. Andriot, and P. Lemerle, "Dynamic balance control of humanoids for multiple grasps and non coplanar frictional contacts," in *Proc. IEEE-RAS Int. Conf. Humanoid Robots*, 2007, pp. 81–88.
- [35] A. Macchietto, V. Zordan, and C. R. Shelton, "Momentum control for balance," ACM Trans. Graph., vol. 28, no. 3, 2009, Art. no. 80.
- [36] K. Bouyarmane and A. Kheddar, "Using a multi-objective controller to synthesize simulated humanoid robot motion with changing contact configurations," in *Proc. IEEE/RSJ Int. Conf. Intell. Robots Syst.*, Sep. 2011, pp. 4414–4419.
- [37] J. Salini, "Dynamic control for the task/posture coordination of humanoids: Toward synthesis of complex activities," Ph.D. dissertation, , Univ. Pierre et Marie Curie, Paris, France, 2012. [Online]. Available: https://tel.archives-ouvertes.fr/tel-00710013/
- [38] S. Caron, Q.-C. Pham, and Y. Nakamura, "Stability of surface contacts for humanoid robots: Closed-form formulae of the contact wrench for rectangular support areas," in *Proc. IEEE Int. Conf. Robot. Autom.*, May 2015, pp. 5107–5112.
- [39] J. Vaillant, K. Bouyarmane, and A. Kheddar, "Multi-character physical and behavioral interactions controller," *IEEE Trans. Vis. Comput. Graph.*, vol. 23, no. 6, pp. 1650–1662, Jun. 2017.
- [40] D. E. Stewart and J. C. Trinkle, "An implicit time-stepping scheme for rigid body dynamics with inelastic collisions and Coulomb friction," *Int. J. Numer. Methods Eng.*, vol. 39, no. 15, pp. 2673–2691, 1996.
- [41] J. Vaillant et al., "Multi-contact vertical ladder climbing with an HRP-2 humanoid," Auton. Robots, vol. 40, no. 3, pp. 561–580, 2016.
- [42] C. Atkeson, "Comparison of Atlas Robot Controllers: IHMC, MIT, and WPI-CMU," Carnegie Mellon Univ., Pittsburgh, PA, USA, Aug. 6, 2017. [Online]. Available: http://www.cs.cmu.edu/cga/drc/atlas-control/
- [43] S. Feng, E. Whitman, X. Xinjilefu, and C. G. Atkeson, "Optimization-based full body control for the DARPA robotics challenge," *J. Field Robot.*, vol. 32, no. 2, pp. 293–312, 2015.

- [44] T. Koolen *et al.*, "Design of a momentum-based control framework and application to the humanoid robot atlas," *Int. J. Humanoid Robot.*, vol. 13, no. 1, 2016, Art. no. 1650007.
- [45] S. Kuindersma et al., "Optimization-based locomotion planning, estimation, and control design for the atlas humanoid robot," Auton. Robots, vol. 40, no. 3, pp. 429–455, 2016.
- [46] S. M. Robinson, "Stability theory for systems of inequalities. Part I: Linear systems," SIAM J. Numer. Anal., vol. 12, no. 5, pp. 754–769, 1975.
- [47] P. Lötstedt, "Perturbation bounds for the linear least squares problem subject to linear inequality constraints," *BIT Numer. Math.*, vol. 23, no. 4, pp. 500–519, 1983.
- [48] J. W. Daniel, "On perturbations in systems of linear inequalities," SIAM J. Numer. Anal., vol. 10, no. 2, pp. 299–307, 1973.
- [49] J. W. Daniel, "Remarks on perturbations in linear inequalities," SIAM J. Numer. Anal., vol. 12, no. 5, pp. 770–772, 1975.
- [50] J. W. Daniel, "Stability of the solution of definite quadratic programs," *Math. Program.*, vol. 5, no. 1, pp. 41–53, 1973.
- [51] 2017. [Online]. Available: https://members.loria.fr/kbouyarmane/multitask_qp_videos
- [52] J. R. Magnus and H. Neudecker, "Matrix differential calculus with applications to simple, Hadamard, and Kronecker products," *J. Math. Psychol.*, vol. 29, no. 4, pp. 474–492, 1985.
- [53] J. R. Magnus and H. Neudecker, "The commutation matrix: Some properties and applications," *Ann. Statist.*, vol. 7, pp. 381–394, 1979.
- [54] D. S. Bernstein, Matrix Mathematics: Theory, Facts, and Formulas. Princeton, NJ, USA: Princeton Univ. Press, 2009.
- [55] J. R. Magnus and H. Neudecker, Matrix Differential Calculus with Applications in Statistics and Econometrics. New York, NY, USA: Wiley, 1999



Abderrahmane Kheddar (M'04–SM'12) received the B.S.C.S. degree from the Institut National d'Informatique (ESI), Algiers, Algeria, and the M.Sc. and Ph.D. degrees in robotics from Pierre and Marie Curie University, Paris, France, in 1990, 1993, and 1997, respectively.

He is currently the Directeur de Recherche with CNRS. He is the Director of the CNRS-AIST Joint Robotic Laboratory, UMI3218/RL, Tsukuba, Japan, and a leader of the Interactive Digital Humans (IDH) team at CNRS-UM

LIRMM, Montpellier, France. His research interests include humanoid robotics, haptics, and thought-based control using brain-machine interfaces.

Dr. Kheddar is a founding member of the IEEE Robotics and Automation Society (RAS) Chapter on Haptics and the co-Chair and co-founding member of the IEEE RAS Technical Committee on model-based optimization. He is an Editor of the IEEE TRANSACTIONS ON ROBOTICS. He is a founding member of the IEEE TRANSACTIONS ON HAPTICS and has served in its editorial board for three years (2007–2010). He is a titular member of the National Academy of Technologies of France and a Knight in the National Order of Merit.



Karim Bouyarmane (M'17) received the double Ingénieur diploma in computer science and applied mathematics from the École Polytechnique, Palaiseau, France, in 2007, and from the École Nationale Supérieure des Mines de Paris, Paris, France, in 2008, and the Ph.D. degree in automatic and microelectronic systems from the University of Montpellier, Montpellier, France, in 2011, after completing the Ph.D. program for full time in the Joint Robotics Laboratory, National Institute of Advanced Industrial Science

and Technology, Tsukuba, Japan.

He was a Japan Society for the Promotion of Science (JSPS) Post-doctoral Fellow with the Advanced Telecommunications Research Institute International, Kyoto, Japan, with the Computational Neuroscience Laboratories, Department of Brain–Robot Interfaces. He also held a CNRS fixed-term researcher position with the Laboratory of Informatics, Robotics and Microelectronics of Montpellier. He is presently an Associate Professor (Maître de Conférences) at the Lorraine Laboratory of Research in Informatics and Applications, Université of Lorraine, Vandœuvre-lès-Nancy, France.